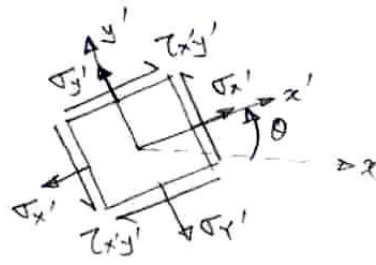
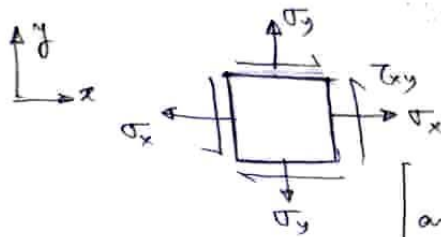


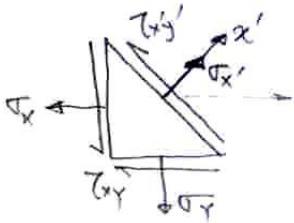
# Stress Transformation

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General relationship

All quantities are positive in both stress blocks



Take Equilibrium  
(Derived in class)

$$\sigma'_x = \sigma_x \cos^2 \theta + \sigma_y \sin^2 \theta + 2\tau_{xy} \sin \theta \cos \theta \quad \dots (1)$$

$$\sigma'_y = \left(\frac{\sigma_x + \sigma_y}{2}\right) - \left(\frac{\sigma_x - \sigma_y}{2}\right) \cos 2\theta + \tau_{xy} \sin 2\theta \quad \dots (2)$$

$$\tau'_x'y' = \tau_{xy} (\cos^2 \theta - \sin^2 \theta) + (\sigma_y - \sigma_x) \sin \theta \cos \theta \quad \dots (3)$$

$$= -\left(\frac{\sigma_x - \sigma_y}{2}\right) \sin 2\theta + \tau_{xy} \cos 2\theta \quad \dots (4)$$

Note:  $\sigma'_y = \sigma'_x(\theta + 90^\circ) = \left(\frac{\sigma_x + \sigma_y}{2}\right) - \left(\frac{\sigma_x - \sigma_y}{2}\right) \cos 2\theta - \tau_{xy} \sin 2\theta$

- Determination of max<sup>m</sup>/min<sup>m</sup> normal stress (i.e. principal stresses) and max<sup>m</sup>/min<sup>m</sup> shearing stress as well as their orientations is simply a maximization/minimization problem.

For example, let us calculate the principal stresses ( $\sigma_1$  &  $\sigma_2$ )

We set  $\frac{d\sigma'_x}{d\theta} = 0 \Rightarrow \tan 2\theta = \frac{\tau_{xy}}{\left(\frac{\sigma_x - \sigma_y}{2}\right)} = \tan 2\theta_p$  (P denotes principal stress planes)

This will give us two values  $\theta_p$  differ by  $90^\circ$ , for  $0 < \theta < 180^\circ$ , These are the two mutually perpendicular principal directions, along which principal stresses ( $\sigma_1, \sigma_2$ ) act.

In order to obtain  $\sigma_1$  &  $\sigma_2$ , we then substitute  $\theta_p$  in (2) as follows:

$$\sin 2\theta_p = \pm \frac{\tau_{xy}}{R} \quad \& \quad \cos 2\theta_p = \pm \frac{\left(\frac{\sigma_x - \sigma_y}{2}\right)}{R} \quad \text{where } R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

Two values of  $\sigma'_x \Rightarrow \sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$

Note:  $\left. \begin{matrix} \sigma_1 > \sigma_2 \\ \uparrow & \uparrow \\ \text{max}^m & \text{min}^m \end{matrix} \right\} \text{ Always true!}$

## Method 1 (DIRECT APPROACH)

Steps:

$\theta$  is always measure from +x axis

### Principal stresses & orientation

$$\frac{d\sigma_{x'}}{d\theta} = 0 \Rightarrow \tan 2\theta_p = \frac{\tau_{xy}}{\frac{\sigma_x - \sigma_y}{2}}$$

obtain two values of  $\theta_p$  differ by  $90^\circ$

Take one value of  $\theta_p$ , plug it in the expression for  $\sigma_{x'}$ , we must obtain any one of the following, defined by the principal stresses ( $\sigma_1, \sigma_2$ ),

$$\sigma_{1,2} = \sigma_{ave} \pm R, \quad \begin{cases} \sigma_{ave} = \frac{\sigma_x + \sigma_y}{2} \\ R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \end{cases}$$

If  $\theta_p$  gives  $\sigma_1$  then call it  $\theta_{p1}$  or  $\theta_p'$   
 "  $\theta_p$  "  $\sigma_2$  " " "  $\theta_{p2}$  or  $\theta_p''$

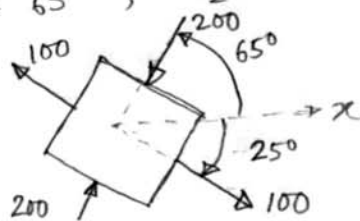
Note:  $\tau_{x'y'} = 0$  for both  $\theta_{p1}$  &  $\theta_{p2}$   
 Thus, there is no shear stress on principal planes

Show the principal stresses in a properly oriented block

Say, for a given values of  $\sigma_x, \sigma_y, \tau_{xy}$  you obtained

$$\theta_{p1} = -25^\circ, \quad \sigma_1 = 100 \text{ MPa}$$

$$\theta_{p2} = 65^\circ, \quad \sigma_2 = -200 \text{ MPa}$$



### Max<sup>m</sup>/Min<sup>m</sup> shearing stress & orientation

$$\textcircled{1} \frac{d\tau_{x'y'}}{d\theta} = 0 \Rightarrow \tan 2\theta_s = -\frac{(\sigma_x - \sigma_y)/2}{\tau_{xy}}$$

obtain two values of  $\theta_s$  differ by  $90^\circ$ . Observe that  $\theta_s = \theta_p \pm 45^\circ$

$\textcircled{2}$  Take any one value of  $\theta_s$ , plug it in the expression for  $\tau_{x'y'}$ , we must obtain any one of the following, defined by max<sup>m</sup>/min<sup>m</sup> shearing stresses ( $\tau_1, \tau_2$ )

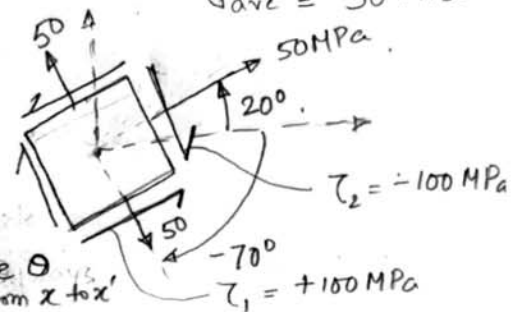
$$\tau_1 = +\tau_{max} \quad \tau_2 = -\tau_{max} \quad \left. \begin{array}{l} \tau_{max} = R \\ = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \\ = \frac{\sigma_1 - \sigma_2}{2} \end{array} \right\}$$

If  $\theta_s$  gives  $\tau_1$  (i.e.  $+\tau_{max}$ ) then call it  $\theta_{s1}$  or  $\theta_{s1}'$ , otherwise  $\theta_{s2}$  or  $\theta_{s2}''$

$\textcircled{3}$  Note:  $\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} = \sigma_{ave}$  for both  $\theta_{s1}$  &  $\theta_{s2}$ . Thus there is an average normal stress in  $\tau_{max}$  (+ & -) planes

$\textcircled{4}$  Show the  $\tau_{max}$  planes  
 Say,  $\theta_{s1} = -70^\circ, \tau_1 = +100 \text{ MPa}$   
 $\theta_{s2} = +20^\circ, \tau_2 = -100 \text{ MPa}$   
 $\sigma_{ave} = 50 \text{ MPa}$

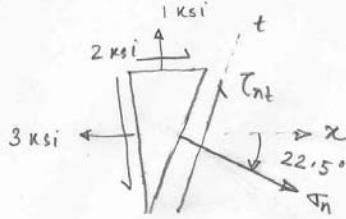
Note:  $\tau_1$  &  $\tau_2$  differ by sign here, since you always look at  $x'$  plane because  $\theta$  is measured from  $x$  to  $x'$



replace  $n$  by  $x'$  and  $t$  by  $y'$  !

Example

(a) Find  $\sigma_n$  and  $\tau_{nt}$  for  $\theta = -22.5^\circ$



Note

$$\left. \begin{aligned} \sigma_x &= 3 \\ \sigma_y &= 1 \\ \tau_{xy} &= 2 \end{aligned} \right\}$$

In the element they are positive according to the sign convention

Use,

$$\sigma_n = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

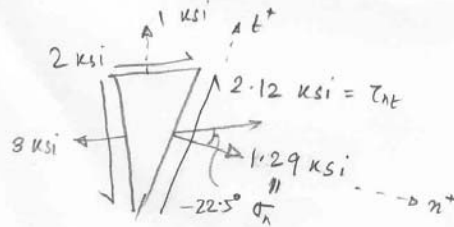
$$\begin{aligned} \sigma_n(-22.5^\circ) &= \frac{3+1}{2} + \frac{3-1}{2} \cos(-45^\circ) + 2 \sin(-45^\circ) \\ &= 2 + 1(0.707) - 2(0.707) = \underline{\underline{1.29 \text{ ksi}}} \end{aligned}$$

$$\tau_{nt} = -\left(\frac{\sigma_x - \sigma_y}{2}\right) \sin 2\theta + \tau_{xy} \cos 2\theta$$

$$= -\left(\frac{3-1}{2}\right) \sin(-45^\circ) + 2 \cos(-45^\circ)$$

$$= 1(0.707) + 2(0.707) = \underline{\underline{2.12 \text{ ksi}}}$$

Both values are positive, so they act in the positive  $n$  and  $t$  directions, as shown below



(b) Find principal stresses ( $\sigma_1$  &  $\sigma_2$ ) and show on stress block w.r.t  $x$ -axis

$$\begin{aligned}\sigma_{1,2} &= \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2} \\ &= \frac{3+1}{2} \pm \sqrt{\left(\frac{3-1}{2}\right)^2 + 2^2} = 2 \pm \sqrt{5}\end{aligned}$$

$$\sigma_1 = \underline{4.25 \text{ ksi}} \quad \text{and} \quad \sigma_2 = \underline{-0.24 \text{ ksi}}$$

Orientation,  $\tan 2\theta_p = \frac{\tau_{xy}}{\left(\frac{\sigma_x - \sigma_y}{2}\right)} = \frac{2}{\left(\frac{3-1}{2}\right)} = 2$

$$\Rightarrow 2\theta_p = 63.43^\circ \text{ and } 243.43^\circ$$

Therefore  $\theta_p = 31.7^\circ$  and  $121.7^\circ$  (both positive, measured cc from  $x$ -axis)

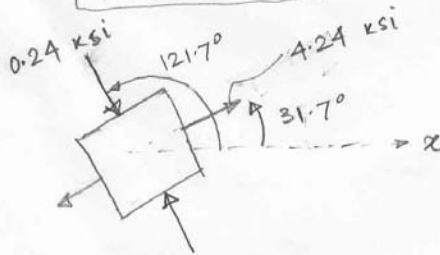
\* Which angle is  $\theta_{p1}$  (gives  $\sigma_1$  plane)?  
& " " is  $\theta_{p2}$  (gives  $\sigma_2$  plane)?

$$\begin{aligned}\text{Try } 31.7^\circ \text{ in } \sigma_n(31.7^\circ) &= \frac{3+1}{2} + \frac{3-1}{2} \cos(63.43^\circ) \\ &\quad + 2 \sin(63.43^\circ) \\ &= \underline{4.24} = \sigma_1 !\end{aligned}$$

Remark - This is a good check also

↑ we obtained this already using direct formula above

Hence,  $\boxed{\begin{aligned}\theta_{p1} &= 31.7^\circ \\ \theta_{p2} &= 121.7^\circ\end{aligned}}$



(C) Find  $\tau_{max}$  and show its plane w.r.t x axis

$$\tau_{max} = \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$= \pm \sqrt{\left(\frac{3-1}{2}\right)^2 + 2^2} = \pm \sqrt{5} = \pm 2.24 \text{ ksi}$$

$$\tan 2\theta_s = - \frac{(\sigma_x - \sigma_y)/2}{\tau_{xy}} = -0.5$$

$$2\theta_s = \tan^{-1}(-0.5) = -26.56^\circ \text{ and}$$

$$-26.56^\circ + 180^\circ = 153.4^\circ$$

therefore  $\theta_{s1} = -13.28^\circ$  and  $76.7^\circ$   
 (measured clockwise) (measured cc)  
 [observe they differ by  $45^\circ$  from  $\theta_p$  !]

Which angle is  $\theta_{s1}$  (gives  $+\tau_{max}$  plane)?  
 & " " is  $\theta_{s2}$  (gives  $-\tau_{max}$  plane)?

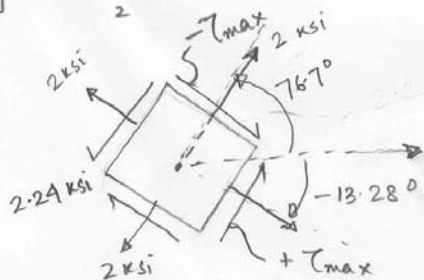
Try  $76.7^\circ$  in  $\tau_{nt}(76.7^\circ) = -\left(\frac{3-1}{2}\right) \sin(153.4^\circ) + 2 \cos(153.4^\circ)$

$$= -2.24 = -\tau_{max}$$

(great!)

Hence  $\theta_{s1} = -13.28^\circ$   
 $\theta_{s2} = 76.7^\circ$

Note,  $\sigma_{avg} = \frac{\sigma_x + \sigma_y}{2} = 2 \text{ ksi}$  (present in max<sup>n</sup> shear stress planes)



Note for  $76.7^\circ$   
 $\tau_{max}$  is negative, means must act along (-) direction