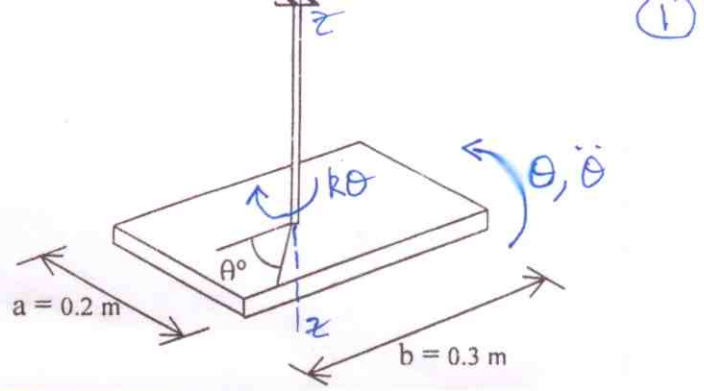


P.61

P.61. A 10 kg rectangular plate, shown in the figure, is suspended at its center from a rod having a torsional stiffness  $k = 1.5 \text{ N.m/rad}$ . Develop the equation of motion for small angular rotation  $\theta$  (in the plane of the plate), and determine the natural period of vibration of the plate.



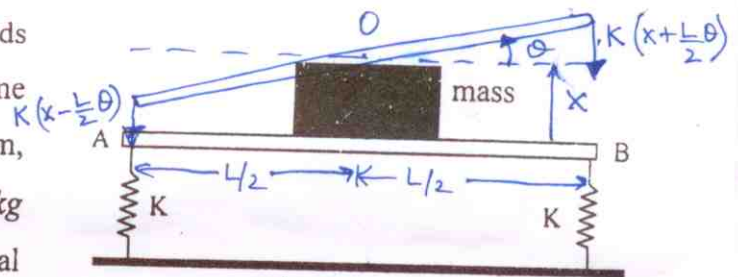
$$I_z \ddot{\theta} = -k\theta \Rightarrow \boxed{\frac{m(a^2+b^2)}{12} \ddot{\theta} + k\theta = 0} \quad \leftarrow \text{EOM (Equation of motion)}$$

$$\Rightarrow \frac{10(0.04+0.09)}{12} \ddot{\theta} + 1.5\theta = 0 \Rightarrow \ddot{\theta} + \omega_n^2 \theta = 0$$

$$\omega_n = \sqrt{\frac{1.5 \times 12}{1.3}} = 3.72 \text{ rad/sec}, \quad T_n = \frac{2\pi}{\omega_n} = 1.689 \text{ sec}$$

P.62

P.62. The uniform beam is supported at its ends by two springs A and B, each having the same stiffness  $k$ . When nothing is supported on a beam, it has a period of vibration of 0.83 s. If a 50 kg mass is placed at its center, the period of vertical vibration is 1.52 s. Compute the stiffness of each spring and the mass of the beam.



$x$  measured from static equilibrium position ( $\delta_{st}$ ) so no need to show  $(M+m)g$  in FBD.

$$\sum F_x = (M+m)\ddot{x} \Rightarrow (M+m)\ddot{x} = -K\left(x - \frac{L}{2}\theta\right) - K\left(x + \frac{L}{2}\theta\right)$$

$$\Rightarrow \boxed{(M+m)\ddot{x} + 2Kx = 0} \rightarrow \text{①} \rightarrow \text{(EOM for } x\text{)}$$

$$\sum M_z = I\ddot{\theta} \Rightarrow \frac{ML^2}{12}\ddot{\theta} = K\left(x - \frac{L}{2}\theta\right)\frac{L}{2} - K\left(x + \frac{L}{2}\theta\right)\frac{L}{2}$$

$$\Rightarrow \boxed{\frac{ML^2}{12}\ddot{\theta} + \frac{KL^2}{4}\theta = 0} \rightarrow \text{②} \rightarrow \text{(EOM for } \theta\text{)}$$

①, ② are the equations of motion for the free-vibration of this 2-dof system. Notice that they are uncoupled (i.e.,  $x, \theta$  appear in separate equations, hence they don't depend on each other). So, for vertical vibrations we need ① only.

$$\text{Given, } m=0, \quad \sqrt{\frac{2K}{M}} = (0.83)^{-1} \times 2\pi$$

$$m=50, \quad \sqrt{\frac{2K}{M+m}} = \sqrt{\frac{2K}{M+50}} = (1.52)^{-1} \times 2\pi$$

$$\Rightarrow \frac{M+50}{M} = \left(\frac{1.52}{0.83}\right)^2 \Rightarrow M = 21.24 \text{ kg}, \Rightarrow K = \frac{M}{2} \left(\frac{2\pi}{0.83}\right)^2 = 608.7 \text{ N/m}^2$$

Note: If we measure vertical displacement from position of undeformed spring, and call it  $y$ , then in place of ① we have,

$$(M+m)\ddot{y} + 2Ky + (M+m)g = 0 \rightarrow \textcircled{3}$$

Put  $\ddot{y} = 0$ , get  $y_{st} = \delta_{st} = -\frac{(M+m)g}{2K}$  (static equilibrium position).  $\rightarrow \textcircled{4}$

Now let  $y = x + \delta_{st} \rightarrow$  insert in ③,

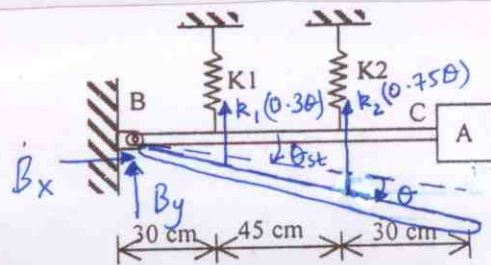
$$(M+m)\ddot{x} + 2K(x + \delta_{st}) + (M+m)g = 0 \rightarrow \textcircled{1} \text{ (solve get back ①)}$$

by virtue of definition of static equilibrium position,  $\delta_{st}$ , i.e., ④ above.

At the static equilibrium position shown in the figure, we have additional spring forces directed upward, equal to  $K\delta_{st}$  on each spring. We have not shown these since they cancel  $(M+m)g$  in the summation of vertical forces ( $\sum F_y$ ), and their moments about  $O$  cancel each other in the sum of moments ( $\sum M_z$ ).

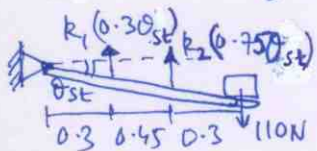
P.63.

P.63. What is the natural frequency of motion for block  $A$  for small oscillation? Consider  $BC$  to have negligible mass and body  $A$  to be a particle. When body  $A$  is attached to the rod, the static deflection is 25 mm. The spring constant  $K_1 = 1.75 \text{ N/mm}$ . Body  $A$  weighs 110 N. What is  $K_2$ ?



static deflection:

$$\sum M_B = 0 \rightarrow K_1 (25 \times \frac{30}{105}) (30) + K_2 (25 \times \frac{75}{105}) (75) = 110 (105) \rightarrow \textcircled{1}$$



$$\Rightarrow K_2 = 8.344 \text{ N/mm} = 8344 \text{ N/m} \blacktriangleleft$$

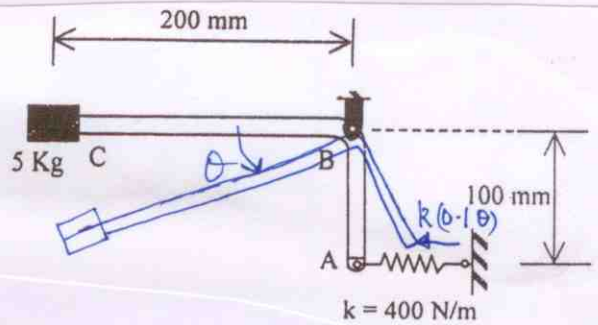
Now if we measure  $\theta$  from static equilibrium position, then due to static equilibrium equation ① we can omit the contribution of 110 N force in moment equation, since it is cancelled out by the LHS terms in ①. Thus the dynamic equilibrium equation, for small  $\theta$ , is

$$\sum M_z = I\ddot{\theta} \Rightarrow -[K_1(0.3\theta)(0.3) + K_2(0.75)(0.75\theta)] = \left(\frac{110}{9.81}\right)(1.05)^2 \ddot{\theta} \rightarrow \text{EOM}$$



$$\omega_n = \sqrt{\frac{0.09k_1 + 0.5625k_2}{\left(\frac{110}{9.81}\right) (1.05)^2}} = 19.809 \text{ rad/s.} \blacktriangleleft$$

**P.64** P.64. The bent rod shown in the figure has negligible mass and supports a 5 kg collar at its end. Develop the equation of a motion and determine the natural period of vibration for the system.



The static equilibrium position is shown, i.e., spring is sufficiently compressed in the position shown so that its force provides a moment about B to balance moment due to collar weight. So, for motion about static equilibrium position, the moment due to 5kg and spring force at static equil cancel each other, hence not shown.

$$\sum M_z = I \ddot{\theta} \Rightarrow \underbrace{5 \cdot (0.2)^2}_{I} \ddot{\theta} = - \underbrace{k(0.1\theta)(0.1)}_{\text{Spring moment}}$$

$$\Rightarrow 0.2 \ddot{\theta} + 4\theta = 0 \quad \text{EoM.}$$

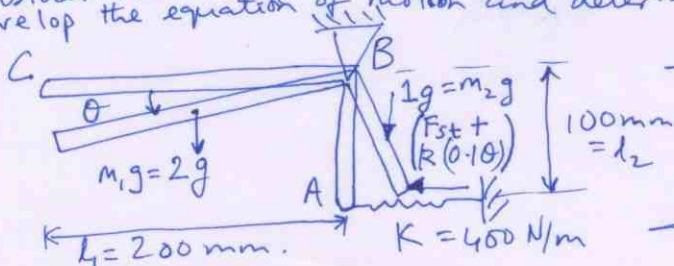
$$\omega_n = \sqrt{\frac{4}{0.2}} = 4.47 \text{ rad/sec.} \blacktriangleleft$$

$$T_n = 2\pi/\omega_n = 1.405 \text{ sec} \blacktriangleleft$$

So  $\theta$  measured from static equilibrium position.

**P.65**

Consider rod ABC (shown in P64) to have uniformly distributed mass of 3 kg. Develop the equation of motion and determine the natural period of vibration for the system. Assume that  $\theta = 0$  is the static equilibrium position.



$$\sum M_B = I_B \ddot{\theta}$$

$$\Rightarrow \left( \frac{m_1 l_1^2}{3} + \frac{m_2 l_2^2}{3} \right) \ddot{\theta} = m_1 g \frac{l_1}{2} - m_2 g \frac{l_2}{2} - (F_{st} + k(0.1\theta)) l_2 \rightarrow ①$$

Static equilibrium equation is,

$$\sum M_B = 0 \rightarrow m_1 g \frac{l_1}{2} - F_{st} l_2 = 0 \rightarrow ②$$

$$② \text{ in } ① \rightarrow \left( \frac{m_1 l_1^2 + m_2 l_2^2}{3} \right) \ddot{\theta} + \left( m_2 g \frac{l_2}{2} + 0.1k \right) \theta = 0$$

EoM.

Here  $2g$  and  $1g$  are the weights of horizontal & vertical legs, respectively.  $F_{st} + k(0.1\theta)$  is static equil spring force + incremental spring force due to small motion  $\theta$  about static equil ( $\theta = 0$ ) position.

can also get this by putting  $\ddot{\theta} = 0$  for static equilibrium and  $\theta = 0$ , i.e. the static equil position in ①

$$\frac{(2 \times 0.2^2 + 1 \times 0.1^2)}{3} \ddot{\theta} + \left(1 \times 9.81 \times \frac{0.1}{2} + 0.1 \times 400\right) \theta = 0$$

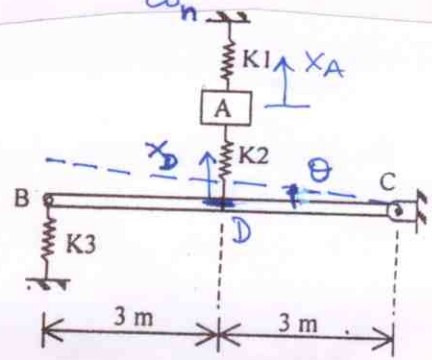
(4)

$$\omega_n = \sqrt{\left(\frac{0.981}{2} + 40\right) / \frac{(2 \times 0.04 + 0.01)}{3}} = 36.74 \text{ rad/sec.} \leftarrow$$

$$\Rightarrow T_n = \frac{2\pi}{\omega_n} = 0.171 \text{ s} \leftarrow$$

P66.

P.66. What are the differential equation of motion about the static equilibrium configuration and the natural frequency of motion of body A for small motion of BC? Neglect inertial effects from BC. Assume  $K_1 = 15 \text{ N/m}$ ,  $K_2 = 20 \text{ N/m}$ ,  $K_3 = 30 \text{ N/m}$  and  $W_A = 30 \text{ N}$ .



Can assume, without loss of generality, that configuration shown is the static equilibrium configuration. Given that BC is massless, (i.e., neglect inertial effects of BC) and for motions about static equilibrium i.e., dropping the weight of A from FBD, we have

①  $m_A \ddot{x}_A = -k_1 x_A - k_2 (x_A - x_D)$   $\xrightarrow{\text{EoM}}$  from vertical dynamic equil of A.

②  $\frac{I_D^{BC}}{D} \ddot{\theta} = -k_3 (6\theta)(6) + k_2 (x_A - x_D)(3)$   $\xrightarrow{\text{EoM}}$  from angular dynamic equil of BC  
 $= 0$  ( $\because$  BC is massless, ie has no inertia).

③  $\theta = x_D / 3$   $\rightarrow$  from kinematics (ie geometry).

③ in ②  $\rightarrow -36k_3 \frac{x_D}{3} + 3k_2 (x_A - x_D) = 0 \Rightarrow x_D = \frac{3k_2}{3k_2 + 12k_3} x_A$

Thus due to inertialess rod BC the apparent 2-dof problem actually reduces to 1-dof problem. (since  $x_D$  depends purely on  $x_A$ ).

④ in ①  $\rightarrow m_A \ddot{x}_A + \left[ k_1 + k_2 \left( \frac{4k_3}{k_2 + 4k_3} \right) \right] x_A = 0$   $\xrightarrow{\text{EoM}}$  for  $x_A$

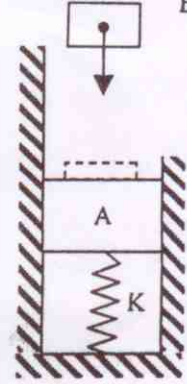
$$\omega_n = \sqrt{\frac{k_1 k_2 + 4k_3 (k_1 + k_2)}{m_A (k_2 + 4k_3)}}$$

$$= 3.242 \text{ rad/sec} \leftarrow$$



P.67

P.67. A rigid body  $A$  rests on a spring with stiffness  $K = 8.80 \text{ N/mm}$ . A lead pad  $B$  falls on to the block  $A$  with a speed on impact of  $7 \text{ m/sec}$ . If the impact is perfectly plastic, what are the frequency and amplitude of the motion of the system, provided that the lead pad sticks to  $A$  at all times? Take  $W_A = 134 \text{ N}$  and  $W_B = 22 \text{ N}$ . What is the distance moved by  $A$  in  $0.02 \text{ s}$ ?



Perfectly plastic impact,  $e=0$  (coeff of restitution), i.e. bodies stick to each other just after impact. During impact momentum is conserved, i.e.,

$$m_B v_B = (m_A + m_B) v \Rightarrow v = \frac{m_B}{(m_A + m_B)} v_B = \text{velocity just after impact. (combined (A+B))}$$

Eqn of motion (EOM) of spring-block system is

$$(m_A + m_B) \ddot{x} + Kx = 0$$

So initial conditions (IC's) are:

$$x_0 \triangleq x(0) = +m_B g / K = 22 / 8800 \text{ m}$$

$$\dot{x}_0 \triangleq \dot{x}(0) = -v = -\frac{m_B}{(m_A + m_B)} v_B = -\frac{154}{156}$$

$x$  measured about static equilibrium, upward (+).

$$x = C \sin(\omega_n t + \psi), \quad C = \left( x_0^2 + \frac{\dot{x}_0^2}{\omega_n^2} \right)^{1/2}, \quad \tan \psi = \frac{x_0 \omega_n}{\dot{x}_0}$$

$$\omega_n = \sqrt{\frac{K}{(m_A + m_B)}} = \sqrt{\frac{8800}{(134 + 22) / 9.81}} = 23.52 \text{ rad/s}$$

$$C = -\sqrt{\frac{(154/156)^2 \times 156 + (22/8800)^2}{8800 \times 9.81}} = -0.042039 \text{ m}, \quad \psi = -0.594933 \text{ rad}$$

$$\text{Amplitude} = |C| = 0.042039 \text{ m}$$

$$x|_{t=0.02 \text{ s}} = -0.016792 \text{ m}$$

$$\text{So, dist moved by } A \text{ in } 0.02 \text{ s} = \frac{22}{8800} - (-0.016792) = 0.019292 \text{ m}$$

NOTE: We fudge the  $-$  sign to make it match initial conditions, i.e.  $x_0 = C \sin \psi$ ,  $\dot{x}_0 = C \omega_n \cos \psi$

$\therefore \sin \psi < 0$ ,  $\cos \psi > 0$ ,  $x_0 > 0$ ,  $\dot{x}_0 < 0$  we must

have  $C < 0$ .

Alternative is to use

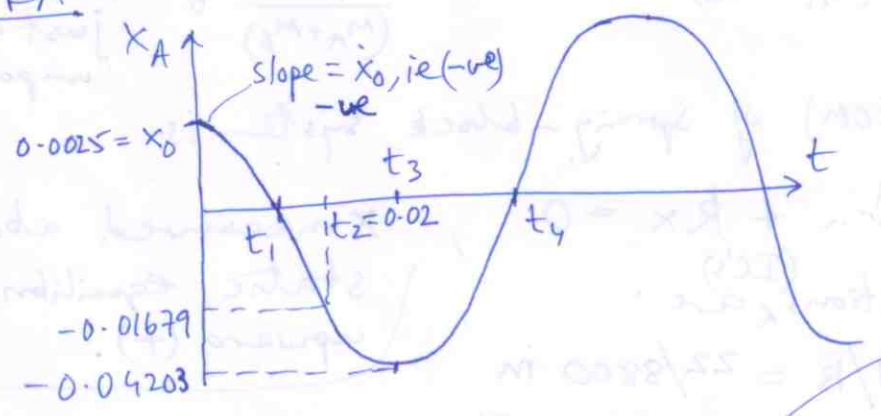
$$x = \underbrace{A}_{x_0} \cos \omega_n t + \underbrace{\frac{\dot{x}_0}{\omega_n}}_{\dot{x}_0/\omega_n} \sin \omega_n t \quad \text{and get}$$

$$x|_{t=0.02} = \frac{22}{8800} \cos(23.52 \times 0.02) + \frac{(-154/156)}{23.52} \sin(23.52 \times 0.02)$$

$$= -0.016795 \text{ m (same as earlier)}$$

⇒ dist moved by A is same as by earlier way.

EXTRA



$$T_n = \frac{2\pi}{\omega_n} = 0.2671 \text{ s}$$

First zero crossing when

$$\omega_n t_1 + \psi = 0$$

$$\Rightarrow t_1 = \frac{-\psi}{\omega_n} = 0.00253 \text{ SECS.}$$

First peak when

$$\omega_n t_3 + \psi = \pi/2$$

$$t_3 = 0.06932 \text{ s.}$$

Second zero crossing,

$$\omega_n t_4 + \psi = \pi$$

$$\Rightarrow t_4 = 0.1361 \text{ s.}$$

So period =  $2(t_4 - t_1)$

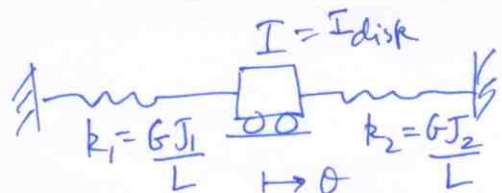
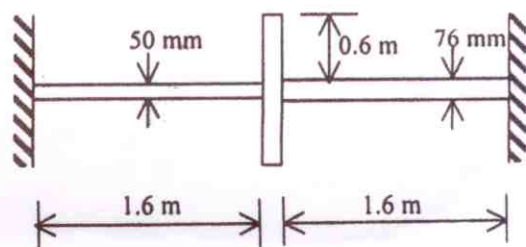
=  $0.2671 \checkmark$

checks out.

$$x(t_3) = \left( \sin(\omega_n t_3 + \psi) \right) = -0.04203 \text{ m}$$



P.68. What is the equivalent torsional spring constant on the disc from the shafts? The modulus of rigidity for the shaft is  $10 \times 10^{10} \text{ N/m}^2$ . What is the natural frequency of the system? If the disc is twisted  $10^\circ$  and then released, what will its angular position be in 1 sec? Neglect the mass of shaft. The disc weighs 143N



Equivalent system

EOM:  $I\ddot{\theta} = -(k_1 + k_2)\theta = -\frac{G}{L}(J_1 + J_2)\theta$

$$I\ddot{\theta} + \frac{G}{L}(J_1 + J_2)\theta = 0$$

$$k_{eq} = \frac{G}{L}(J_1 + J_2) = \frac{10^{11}}{1.6} \times \frac{\pi}{32} \left( \left[ \frac{50}{1000} \right]^4 + \left[ \frac{76}{1000} \right]^4 \right) = 243057.3 \text{ N.m/rad}$$

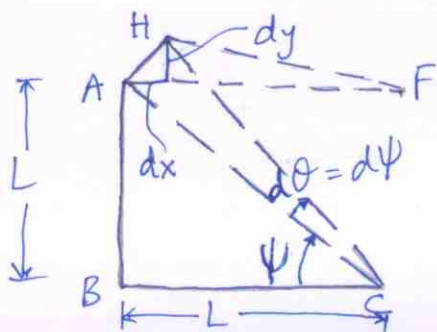
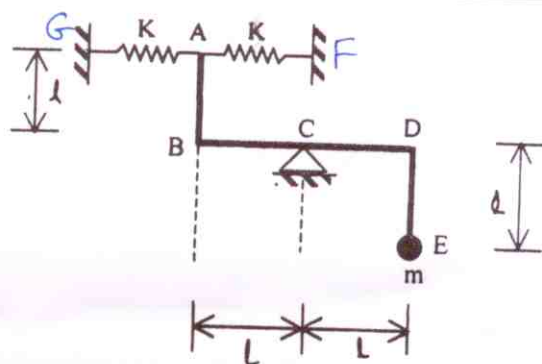
$$\omega_n = \sqrt{\frac{G(J_1 + J_2)}{L I}} = \sqrt{\frac{k_{eq}}{\frac{143}{9.81} \frac{0.6^2}{2}}} = 304.36 \text{ rad/sec}$$

IC's:  $\theta_0 \triangleq \theta(0) = 10^\circ \frac{\pi}{180} = 0.1745$ ,  $\dot{\theta}_0 \triangleq \dot{\theta}(0) = 0 \text{ rad/sec}$

$$C = \left[ \theta_0^2 + \left( \frac{\dot{\theta}_0}{\omega_n} \right)^2 \right]^{1/2} = \frac{\pi}{18}, \quad \psi = \tan^{-1} \left( \frac{\dot{\theta}_0 \omega_n}{\theta_0} \right) = \tan^{-1}(0) = \frac{\pi}{2}$$

$$\theta \Big|_{t=1 \text{ sec}} = C \sin \left[ \omega_n (1) + \frac{\pi}{2} \right] = -0.1623 \text{ rad} = -9.3^\circ$$

P.69. a) If bar ABCDE is of negligible mass, what is the natural frequency of free oscillation of the system for small amplitude of motion? Take  $K = 25 \text{ N/m}$ ,  $m = 2 \text{ kg}$ ,  $l = 1 \text{ m}$ . b) If mass of bar ABCDE is  $0.4 \text{ kg/m}$ , what is the natural frequency of free oscillation of the system for small amplitude of motion? Take  $K = 25 \text{ N/m}$ ,  $m = 2 \text{ kg}$ ,  $l = 1 \text{ m}$ .



$$AF = L$$

$$HF = \sqrt{(L - dx)^2 + (dy)^2} = \sqrt{L^2 - 2Ldx + (dx)^2 + (dy)^2}$$

$$= L \left( 1 - \frac{dx}{L} + \frac{1}{2} \left\{ \left( \frac{dx}{L} \right)^2 + \left( \frac{dy}{L} \right)^2 \right\} + \text{HOT's} \right)$$

neglect (higher order terms).

$$= L - dx.$$

So compression of spring AF is  $(AF - HF) = dx$   
Likewise, extension of " AG is  $(GH - GA) = dx$ .

We could have guessed this directly, i.e., for small motions the change in length of a spring equals (nearly) its component along the original direction of the spring.

Now for small motion, B essentially moves vertically and A horizontally. Thus  $dx = Ld\theta$ .  
Alternatively, a cleaner (non graphical) way to get this is as follows. Let  $x$  be <sup>horizontal</sup> coordinate of measured from C.

$$x = -AC \cos\psi \Rightarrow dx = AC \sin\psi d\psi = Ld\theta$$

Now replace  $dx, d\theta$  with  $x, \theta$  thruout (i.e.  $x, \theta$  are small).

Also note that position shown can be assumed as static equilibrium position, so in this position the moments <sub>about C</sub> due to spring forces balance that due to self-weight hence <sub>self-wt</sub> is not accounted in EOM about static equilibrium (as usual).

(a)  $I_C \ddot{\theta} = \sum M_C \Rightarrow m(\sqrt{2}L)^2 \ddot{\theta} = -2K(L\theta)(L)$   
 $2mL^2 \ddot{\theta} + 2KL^2 \theta = 0$   
 $\omega_n = \sqrt{K/m} = \sqrt{25/2} = 3.5355 \text{ rad/sec}$

(b) Only  $I_C$  changes here. (Compare with P.65 where part of self-wt had to be accounted for in EOM).

$$I_C = \left[ (2SL) \frac{(2L)^2}{12} \right] + \left[ 2 \left\{ (SL) \frac{L^2}{12} + (SL) \left( \frac{L^2}{4} + L^2 \right) \right\} + m(2L^2) \right]$$

$I_{BC}$        $I_{AB} + I_{DE}$

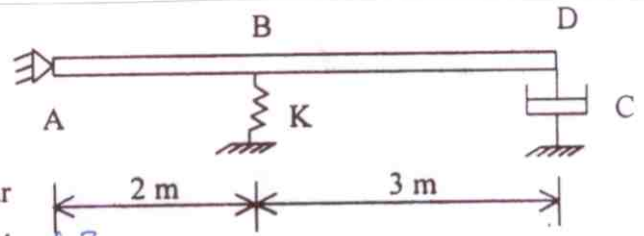
$$\Rightarrow I_C = 5.333 \text{ kgm}^2 \Rightarrow \omega_n = \sqrt{\frac{2KL^2}{I_C}} = \sqrt{\frac{50}{5.33}} = 3.062 \text{ rad/sec}$$



P.70

8

P.70. Derive equation of motion for small rotation the rigid uniform beam of mass 12kg. Take  $K=2500$  N/m,  $C=8$  Kg/sec. What is the damping ratio? If initial rotation of 0.1 rad at A is applied and the bar is released, compute the displacement at D at the end of 3sec.



$$I_A \ddot{\theta} = \sum M_A \Rightarrow \frac{12}{3} \ddot{\theta} = -2500(2\theta)(2) - (5\dot{\theta})(5)$$

$$\Rightarrow 100\ddot{\theta} + 200\dot{\theta} + 10000\theta = 0$$

$$m \ddot{\theta} + c \dot{\theta} + k \theta = 0$$

$$\zeta = \frac{c}{2m\omega_n} = \frac{2}{2 \times 1 \times \sqrt{100/1}} = 0.1$$

$$\theta_0 = 0.1 \text{ rad}, \dot{\theta}_0 = 0$$

$$\theta = (A \cos \omega_d t + B \sin \omega_d t) e^{-\zeta \omega_n t}$$

$$A = \theta_0 = 0.1, B \omega_n \sqrt{1-\zeta^2} - \omega_n \zeta A = \dot{\theta}_0 = 0$$

$$\Rightarrow B = \frac{\zeta A}{\sqrt{1-\zeta^2}} = \frac{0.1 \times 0.1}{\sqrt{1-0.01}} = 0.0100503$$

$$\omega_d = \omega_n \sqrt{1-\zeta^2} = 10 \sqrt{0.99}$$

$$\theta|_{3 \text{ sec}} = \left\{ 0.1 \cos [10 \sqrt{0.99} \times 3] + \frac{0.01}{\sqrt{0.99}} \sin [10 \sqrt{0.99} \times 3] \right\} e^{-0.1 \sqrt{100} \times 3}$$

$$\theta[3] = -0.000478005 \text{ rad} = -0.02739^\circ$$

(or) by alternate approach,

$$\theta = C \sin(\omega_d t + \psi) e^{-\zeta \omega_n t}$$

$$C = \left[ \theta_0^2 + \left( \frac{\dot{\theta}_0 + \zeta \omega_n \theta_0}{\omega_d} \right)^2 \right]^{1/2} = \left[ 0.1^2 + \left( \frac{0.1 \times 10 \times 0.1}{10 \sqrt{0.99}} \right)^2 \right]^{1/2}$$

$\therefore \sin \psi > 0$   
 $\theta_0 > 0$   
 $\Rightarrow C > 0$

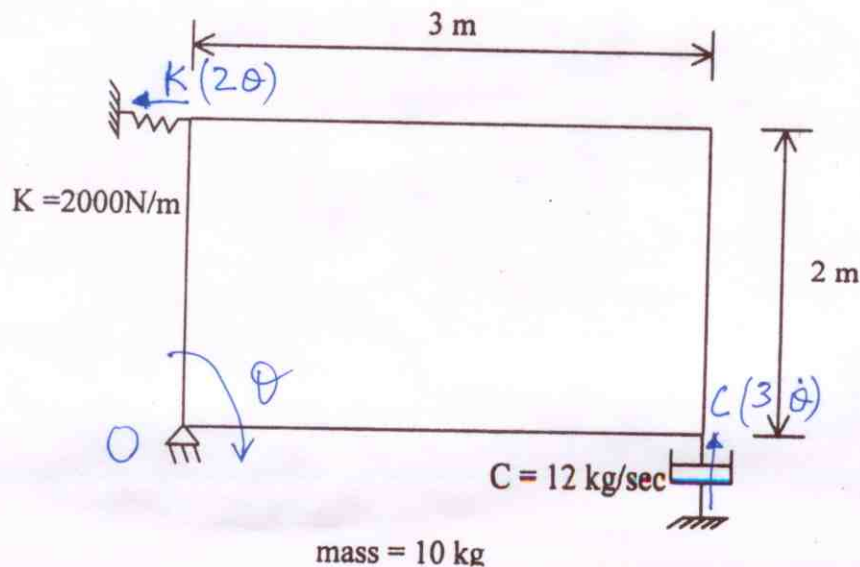
$$\psi = \tan^{-1} \left( \frac{\dot{\theta}_0 \omega_d}{\dot{\theta}_0 + \zeta \omega_n \theta_0} \right) = \tan^{-1} \left( \frac{0.1 \times 10 \times \sqrt{0.99}}{0.1 \times 10 \times 0.1} \right) = 84.26^\circ = 1.4706289$$

$$\theta[3] = 0.100503 \sin(10 \sqrt{0.99} \times 3 + 1.4706289) e^{-0.1 \sqrt{100} \times 3}$$

$$= -0.000478005 \text{ rad} = -0.02739^\circ$$

P.71

P.71. For the rigid, uniform plate shown in the diagram, derive equation of motion for small oscillation.



Assume static equilibrium position shown. (no  $mg$  term in  $\Sigma M_o$ ).

$$I_o \ddot{\theta} = \Sigma M_o$$

$$\left[ m \left( \frac{a^2 + b^2}{12} \right) + m \left( \frac{a^2}{4} + \frac{b^2}{4} \right) \right] \ddot{\theta} = -K(2\theta)(2) - C(5\dot{\theta})(5)$$

$$10 \left( \frac{3^2}{3} + \frac{2^2}{3} \right) \ddot{\theta} + (2000 \times 4) \theta + (12 \times 25) \dot{\theta} = 0$$

$$\Rightarrow \frac{130}{3} \ddot{\theta} + 300 \dot{\theta} + 8000 \theta = 0 \quad \blacktriangleleft$$

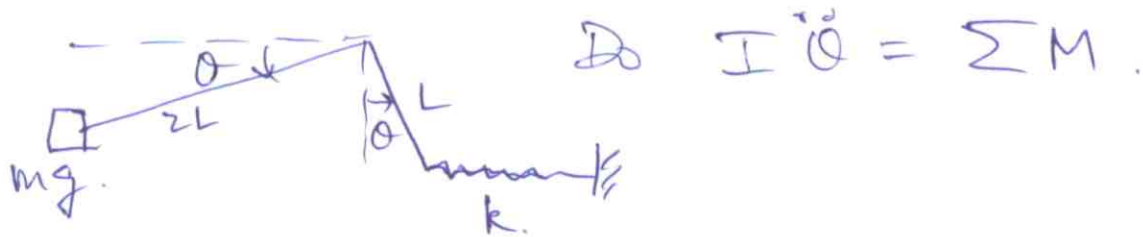


# P64 Modified

Assume given position is undeformed springs.

Assume (as before) that spring is long so essentially it stays horizontal.

Do moment (dynamic) equilibrium.



$$m(2L)^2 \ddot{\theta} = mg 2L \cos \theta - k L \sin \theta L \cos \theta \rightarrow (1)$$

Static equilibrium: Put  $\frac{d(\cdot)}{dt} = \frac{d^2(\cdot)}{dt^2} = 0$ .

$$mg 2L \cos \theta_{st} - k L^2 \sin \theta_{st} \cos \theta_{st} = 0 \rightarrow (2)$$

$$\theta_{st} = \frac{\pi}{2}, \sin^{-1} \left( \frac{mg 2L}{k L^2} \right) \rightarrow (3)$$

## STABILITY OF EQUILIBRIUM.

From energy methods, to find stability of equilibrium

$$V = -mg 2L \sin \theta + \frac{1}{2} k (L \sin \theta)^2$$

$$\frac{dV}{d\theta} = [-mg 2L \cos \theta + k L^2 \sin \theta \cos \theta] = 0$$

gives same  $\theta_{st}$  as (3) above

$$\frac{d^2V}{d\theta^2} = \left[ mg 2L \sin \theta + \frac{k L^2}{2} \cos 2\theta \right]$$

$$\text{For } \theta_{st} = \frac{\pi}{2}, \left. \frac{d^2V}{d\theta^2} \right|_{\theta_{st} = \frac{\pi}{2}} = 2mgL - kL^2$$

So  $\theta_{st} = \frac{\pi}{2}$  is stable for  $2mgL > kL^2$

So when  $\theta_{st1}$  is stable,  $\theta_{st2}$  is not real (11)  
(ie does not exist)

$$\begin{aligned} \left. \frac{d^2V}{d\theta^2} \right|_{\theta_{st2}} &= 2mgL \frac{mg2L}{kL^2} + kL^2 \left[ 1 - 2 \left( \frac{mg2L}{kL^2} \right)^2 \right] \\ &= kL^2 + \frac{2mgL}{kL^2} \left[ 2mgL - 2kL^2 \left( \frac{2mgL}{kL^2} \right) \right] \\ &= kL^2 - \frac{(2mgL)(2mgL)}{kL^2} \end{aligned}$$

$$> 0 \text{ if } 2mgL < kL^2$$

So  $\theta_{st2}$  is stable when it exists (ie is real) <sup>when it</sup>

### SMALL MOTIONS ( $\alpha$ ) ABOUT $\theta_{st}$ (NON-TRIVIAL)

So we want to write the linearized equations for small motion ( $\alpha$ ) about a non-trivial (ie non-zero)  $\theta_{st}$ .

Put  $\theta = \theta_{st} + \alpha$  in (1) & linearize (ie retain only first order terms in  $\alpha$  in the Taylor series expansions of  $\sin \theta$  and  $\cos \theta$ , where  $\alpha$  is small).

$$\left. \begin{aligned} \text{So, } \ddot{\theta} &= \ddot{\theta}_{st} + \ddot{\alpha} = \ddot{\alpha} \\ \sin \theta &= \sin \theta_{st} + \cos \theta_{st} \alpha \\ \cos \theta &= \cos \theta_{st} - \sin \theta_{st} \alpha \end{aligned} \right\} \rightarrow \text{substitute in (1).}$$

So we get,

$$m(2L)\ddot{\alpha} = mg2L(\cos \theta_{st} - \sin \theta_{st} \alpha) - \frac{kL^2}{2}(\sin 2\theta_{st} + 2\cos 2\theta_{st} \alpha) \rightarrow (4)$$



Now use (2) in (4), & see that the (12) double-underlined terms cancel out (since they represent (2), i.e. static equil equation). Thus (4) becomes,

$$m(2L)^2 \ddot{\alpha} = -\left(2mgL \sin \theta_{st} + \frac{kL^2}{2} 2\cos 2\theta_{st}\right) \alpha$$

$$m(2L)^2 \ddot{\alpha} + \left(2mgL \sin \theta_{st} + \frac{kL^2}{2} 2\cos 2\theta_{st}\right) \alpha = 0.$$

↳ simple harmonic oscillator. (5)

### Specializations of Modified problem

(i)  $\theta_{st1} = 90^\circ \rightarrow$  small motions about this.

$$m(2L)^2 \ddot{\alpha} + (2mgL - kL^2) \alpha = 0.$$

this coefficient is  $> 0$ , so stable vibrations.

(ii)  $\theta_{st2} \rightarrow$  small motions about this.  
 (assume  $\theta_{st2}$  is real, i.e. exists),  
 (i.e.,  $mg2L < kL^2$ ).

$$m(2L)^2 \ddot{\alpha} + \left(kL^2 - \frac{(2mgL)^2}{kL^2}\right) \alpha = 0.$$

positive.

Recall solution of original problem (64):

$\theta_{st} = 0$ , and

$$(2L)^2 \ddot{\theta} + kL^2 \theta = 0 \quad \text{for small } \theta, \text{ see p3 of notes.}$$

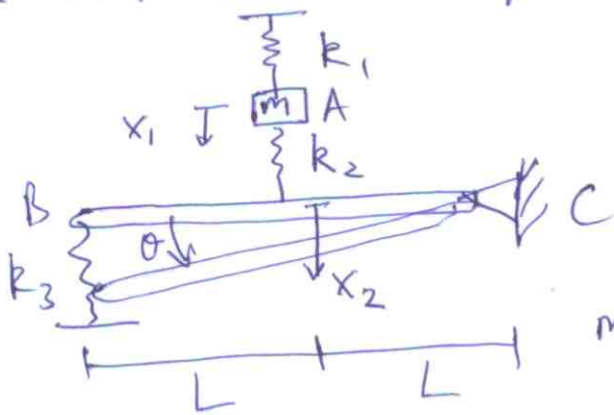
↳ Note: If you put  $\theta_{st} = 0$ ,  $\theta = \theta_{st} + \alpha$ ,  $\alpha$  small in (5) and linearize, you get same result - coincidence.

ie, consistent with  $\theta_{st} = 0$  in (64)

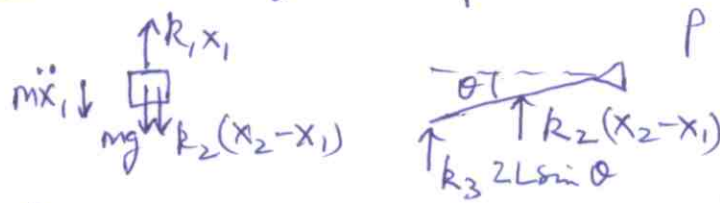
# P.66 Modified.

Assume given position is undeformed springs.

Assume (as before) that all springs are long so essentially they remain vertical. Do translational equilibrium for mass A & rotational equilibrium for rod.



(Note:  $x_1 = -x_A$ ,  $x_2 = -x_D$  in the notation of original problem - see p.4)



$$m \ddot{x}_1 = mg - k_1 x_1 + k_2 (x_2 - x_1) \rightarrow (1)$$

$$\frac{I}{rod} \ddot{\theta} = -k_3 (2L \sin \theta) (2L \cos \theta) - k_2 (x_2 - x_1) L \cos \theta$$

$\theta = 0$  (massless rod).  $x_2 = L \sin \theta \rightarrow (3)$  (from kinematics).  $\rightarrow (2)$

Substitute (3) in (1):

$$m \ddot{x}_1 = mg - k_1 x_1 + k_2 (L \sin \theta - x_1) \rightarrow (4)$$

$$\text{From (3) in (2), } -L \cos \theta [4k_3 L \sin \theta + k_2 (L \sin \theta - x_1)] = 0.$$

$\therefore \cos \theta \neq 0$  in general (note we are not finding  $\theta$  as yet),

$$\text{we get, } \sin \theta = \frac{k_2}{L(4k_3 + k_2)} x_1 \rightarrow (4)$$

Relation (3) is a purely kinematical relation. Relation (4) is a relation arising from (3) & dynamics (2), with  $I_{rod} = 0$ .



Both (3), (4) valid for all 't'.

(14)

Substitute (4) in (3), get,

$$m\ddot{x}_1 + \left[ k_1 + k_2 - \frac{k_2^2}{4k_3 + k_2} \right] x_1 - mg = 0.$$

$$m\ddot{x}_1 + \left[ k_1 + \frac{4k_2k_3}{4k_3 + k_2} \right] x_1 - mg = 0 \rightarrow (5)$$

### STATIC EQUILIBRIUM.

In (5) put  $\frac{d(\cdot)}{dt} = \frac{d^2(\cdot)}{dt^2} = 0$ , get,

$$(x_1)_{st} = \frac{mg}{\left[ k_1 + \frac{4k_2k_3}{4k_3 + k_2} \right]} = \frac{30}{\left( 15 + \frac{4 \times 20 \times 30}{4 \times 30 + 20} \right)}$$
$$= \frac{30}{32.14} = 0.9333$$

$$(\theta)_{st} = \sin^{-1} \left[ \frac{k_2}{L(4k_3 + k_2)} (x_1)_{st} \right] = \sin^{-1} \left[ \frac{20 \times 0.9333}{3 \times (4 \times 30 + 20)} \right]$$

$$\sin^{-1}(0.04444)$$

### SMALL MOTIONS ABOUT EQUILIBRIUM.

put  $x_1 = (x_1)_{st} + x$ , where  $x$  is small,  
in (5) and use (6). You get,

$$m\ddot{x} + \left[ k_1 + \frac{4k_2k_3}{4k_3 + k_2} \right] \left[ \underline{(x_1)_{st}} + x \right] - \underline{mg} = 0$$

underlined terms cancel due to (6), so,

$$m\ddot{x} + \left[ k_1 + \frac{4k_2k_3}{4k_3 + k_2} \right] x = 0$$

↳ Simple harmonic oscillator same result as in  
So vibration of mass A unaffected by static equl (page (4) in this case).