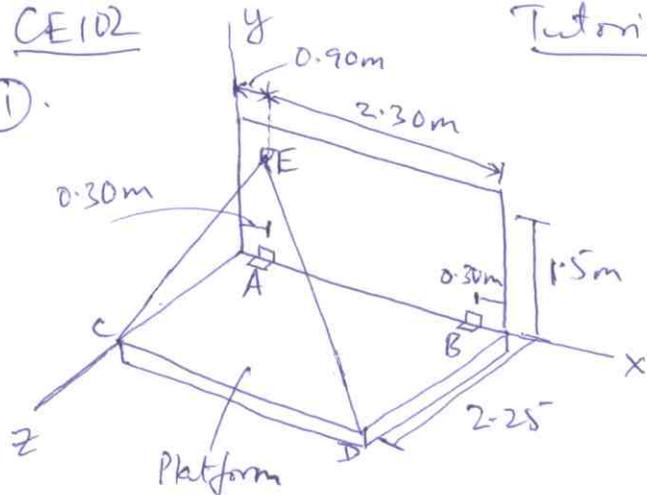


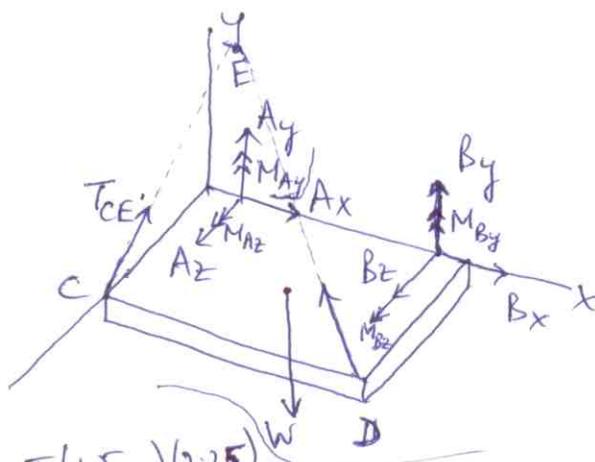
①



Frictionless hook $\Rightarrow T_{CE} = T_{DE} = T$
+ massless rope

$$T_{CE} = T(0.9\mathbf{i} + 1.5\mathbf{j} - 2.25\mathbf{k}) / 2.85$$

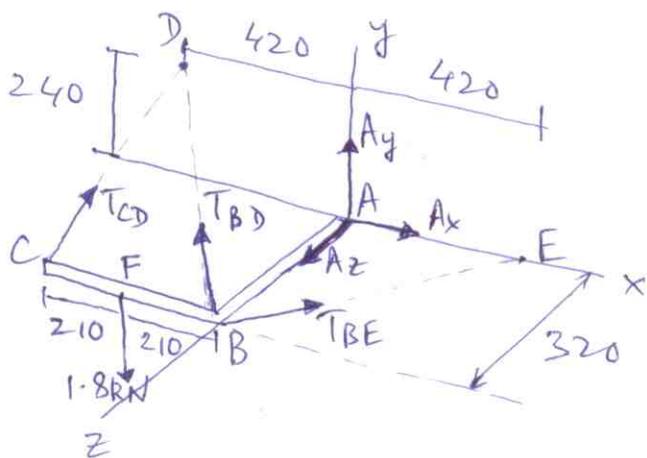
$$T_{DE} = T(-2.3\mathbf{i} + 1.5\mathbf{j} - 2.25\mathbf{k}) / 3.55$$



$$\sum M_{xx} = 0 \Rightarrow T\left(\frac{1.5}{2.85}\right)(2.25) + T\left(\frac{1.5}{3.55}\right)(2.25) - W\left(\frac{2.25}{2}\right) = 0 \Rightarrow T = 1292.35 \text{ N}$$

Longer way: 11 unknowns $(A_x, A_y, A_z, B_x, B_y, B_z, T)$ & 6 eqns
So S.I.D. But you can write $\sum \mathbf{M} = 0, \sum \mathbf{F} = 0$
and solve for T (and some of the reactions).

②



6 unknowns $(A_x, A_y, A_z, T_{BE}, T_{BD}, T_{CD})$

\Rightarrow S.D.

$$T_{CD} = (240\mathbf{j} - 320\mathbf{k}) / 400$$

$$T_{BD} = (-420\mathbf{i} + 240\mathbf{j} - 320\mathbf{k}) / 580$$

$$T_{BE} = (420\mathbf{i} - 320\mathbf{k}) / \sqrt{278800}$$

$\sum M_{AB} = 0$: only T_{CD} participates (besides load).

$$\Rightarrow T_{CD} \left(\frac{240}{400}\right)(420) - 1.8(210) = 0 \Rightarrow T_{CD} = 1.5 \text{ kN} \blacktriangleleft$$

$\sum M_{xx} = 0$: only T_{BD} participates (besides T_{CD} & load).

$$\Rightarrow T_{CD} \left(\frac{240}{400}\right)(320) + T_{BD} \left(\frac{240}{580}\right)(320) - 1.8(320) = 0 \Rightarrow T_{BD} = 2.175 \blacktriangleright$$

$\sum M_{AD} = 0$: only T_{BE} participates (besides load).

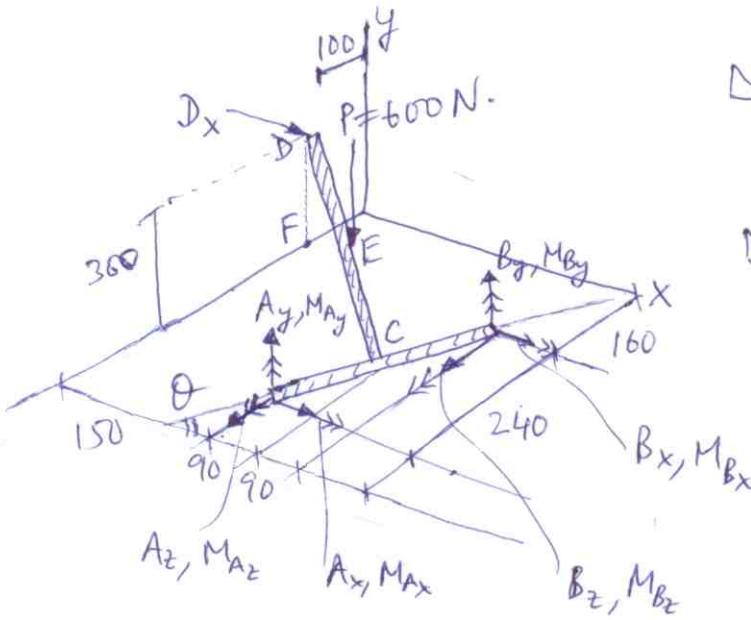
$$\Rightarrow \underline{r}_{AD} \cdot [\underline{r}_{AF} \times (-1.8\mathbf{j}) + \underline{r}_{AB} \times T_{BE}] = 0$$

$$\Rightarrow \frac{(-420\mathbf{i} + 240\mathbf{j})}{\sqrt{234000}} \cdot \left[(-210\mathbf{i} + 320\mathbf{k}) \times (-1.8\mathbf{j}) + T_{BE} \frac{(320\mathbf{k}) \times (420\mathbf{i} - 320\mathbf{k})}{\sqrt{278800}} \right] = 0$$

$$\left(\frac{-420}{\sqrt{234000}} \right) (\cancel{320} \times 1.8) + T_{BE} \left(\frac{240}{\sqrt{234000}} \right) \left(\frac{\cancel{320} \times 420}{\sqrt{278800}} \right) = 0$$

$$\Rightarrow T_{BE} = 3.9601 \text{ kN} \quad \blacktriangleleft$$

③



NOTE: $(M_{Ax}\mathbf{i} + M_{Az}\mathbf{k}) \cdot \underline{e}_{AB} = 0$

$(M_{Bx}\mathbf{i} + M_{Bz}\mathbf{k}) \cdot \underline{e}_{AB} = 0$

NOTE: If either of the bearings at A or B do not provide axial thrust, then for that bearing the x and z comp of reaction are related such that their sum has no comp along \underline{e}_{AB} .

NOTE: only one of the bearings at A or B is required to provide axial thrust to balance the comp of D_x along \underline{e}_{AB} / NOTE: S.I.D \therefore reactions > 6 .

$\Sigma M_{AB} = 0$ gives $D_x \therefore$ only D_x participates (besides P).

$$\Rightarrow D_x \sin\theta (300) - P \left(\frac{d}{2} \right) = 0$$

where $d = \perp^{\text{ar}}$ dist from F to AB.

$$\underline{AF} = -150\mathbf{i} - (240 + 160 - 100)\mathbf{k} = -150\mathbf{i} - 300\mathbf{k}$$

$$\underline{e}_{AB} = (180\mathbf{i} - 240\mathbf{k}) / 300 = 0.6\mathbf{i} - 0.8\mathbf{k}$$

$$d = \sqrt{(\underline{AF})^2 - (\underline{AF} \cdot \underline{e}_{AB})^2} = \sqrt{112500 - (-150 \times 0.6 + 300 \times 0.8)^2}$$

$$= 300$$

$$\Rightarrow D_x = 600 \left(\frac{300}{2} \right) / (300(0.8)) = 375 \text{ N}$$

Can also do by vector approach, i.e.,

$$\Sigma M_{AB} = \underline{e}_{AB} \cdot \left[\underline{r}_{AD} \times D_x \mathbf{i} + \underline{r}_{AF} \times (-P \mathbf{j}) \right] \rightarrow \text{will give the result}$$

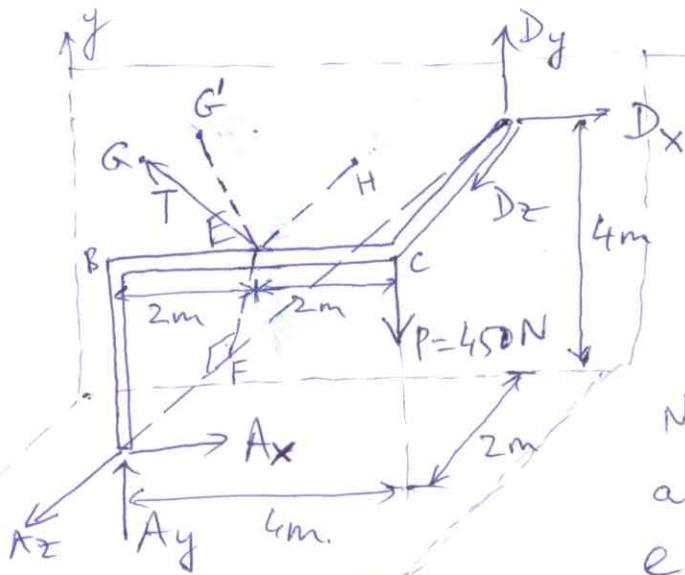
unit vector along AB

$$\theta = \tan^{-1} \left(\frac{240}{180} \right) = 53.13^\circ$$

$$AB = 300 \text{ m}$$

$$\sin\theta = \frac{240}{300} = 0.8$$

(4)



(METHOD 1 - more physical) (3)

7 reactions (3 each at A & D + tension T)
So SFD.

To find T do $\sum M_{AD} = 0$
Now consider three \perp directions at pt E defined by \underline{e}_{EH} , \underline{e}_{EF} , $\underline{e}_{EG'}$, where \underline{e}_{EH} is parallel to \underline{e}_{AD} , as shown.

Then only the $\underline{e}_{EG'}$ component of T contributes to moment about AD axis, so T will be minimum if G coincides with G' (since then T will be wholly in $\underline{e}_{EG'}$ direction so the \underline{e}_{EF} and \underline{e}_{EH} comp's of T are zero, and hence not wasted during ^{process of} providing equilibrium).

$$\underline{e}_{AD} = (4\underline{i} + 4\underline{j} - 2\underline{k})/6 = \frac{2}{3}\underline{i} + \frac{2}{3}\underline{j} - \frac{1}{3}\underline{k} = \underline{e}_{EH}$$

$$AF = \underline{AE} \cdot \underline{e}_{AD} = (2\underline{i} + 4\underline{j}) \cdot \left(\frac{2}{3}\underline{i} + \frac{2}{3}\underline{j} - \frac{1}{3}\underline{k}\right) = \frac{4}{3} + \frac{8}{3} = 4$$

$$AD = \sqrt{4^2 + 4^2 + 2^2} = 6, \Rightarrow DF = AD - AF = 2.$$

$$x_F = \frac{(y_A - y_D) \cdot 2/6}{-4 - 0} = -4/3, \quad y_F = \frac{(x_A - x_D) \cdot 2/6}{-4 - 0} = -4/3, \quad z_F = \frac{(z_A - z_D) \cdot 2/6}{0 - 0} = 2/3$$

$$F \Rightarrow (-4/3, -4/3, 2/3)$$

$$\underline{e}_{EF} = \left[\left(-\frac{4}{3} + 2\right)\underline{i} - \frac{4}{3}\underline{j} + \left(\frac{2}{3} - 2\right)\underline{k} \right] / 2 = \frac{1}{3}\underline{i} - \frac{2}{3}\underline{j} - \frac{2}{3}\underline{k}$$

$$\underline{e}_{EG'} = \underline{e}_{EH} \times \underline{e}_{EF} = \begin{bmatrix} \left(\frac{2}{3}\right)\left(-\frac{2}{3}\right) - \left(-\frac{1}{3}\right)\left(-\frac{2}{3}\right) \\ \left(-\frac{1}{3}\right)\left(\frac{1}{3}\right) - \left(-\frac{2}{3}\right)\left(-\frac{2}{3}\right) \\ \left(\frac{2}{3}\right)\left(-\frac{2}{3}\right) - \left(\frac{2}{3}\right)\left(\frac{1}{3}\right) \end{bmatrix} = \begin{bmatrix} -\frac{6}{9} \\ \frac{3}{9} \\ -\frac{6}{9} \end{bmatrix}$$

$$\underline{e}_{EG'} = -\frac{2}{3}\underline{i} + \frac{1}{3}\underline{j} - \frac{2}{3}\underline{k}$$

parametric form of
So, equation of line through E and in direction of $\underline{e}_{EG'}$ is,
 $\underline{r} = \left(a - \frac{2}{3}t\right)\underline{i} + \left(b + \frac{1}{3}t\right)\underline{j} + \left(c - \frac{2}{3}t\right)\underline{k}$ (\rightarrow gives $\frac{d\underline{r}}{dt} = \underline{e}_{EG'}$).

Say $t=0$ at point E (where t is the parameter),

(4)

$$\Rightarrow a = -2, b = 0, c = 2$$

$$\Rightarrow \underline{r} = (2 - \frac{2}{3}t)\underline{i} + \frac{1}{3}t\underline{j} + (2 - \frac{2}{3}t)\underline{k}$$

for $z=0$ (ie point of intersection, G' , of line r with the wall)

$$2 - \frac{2}{3}t = 0 \Rightarrow t = 3.$$

$$\Rightarrow x = -2 - \frac{2}{3}(3) = -4, \quad y = \frac{1}{3}(3) = 1$$

$$\Rightarrow G' \rightarrow (-4, 1, 0) \text{ for } T_{\min} \quad \blacktriangleleft$$

$$\underline{T} = T_{\min} \left(-\frac{2}{3}\underline{i} + \frac{1}{3}\underline{j} - \frac{2}{3}\underline{k} \right) \quad (\text{ie } T_{\min} \underline{e}_{EG'})$$

$$\Sigma M_{AD} = 0 \Rightarrow \underline{e}_{AD} \cdot [\underline{r}_{AE} \times \underline{T} + \underline{r}_{AC} \times (-P\underline{j})] = 0 \quad \rightarrow (*)$$

$$\Rightarrow \left(\frac{2}{3}\underline{i} + \frac{2}{3}\underline{j} - \frac{1}{3}\underline{k} \right) \cdot \left[(2\underline{i} + 4\underline{j}) \times \left(-\frac{2}{3}\underline{i} + \frac{1}{3}\underline{j} - \frac{2}{3}\underline{k} \right) T_{\min} - P(4\underline{i} + 4\underline{j}) \times (\underline{j}) \right] = 0.$$

$$(\text{ie } T_{\min} * EF)$$

$$\Rightarrow T_{\min} \sqrt{20-16} = \frac{4}{3}P \Rightarrow T_{\min} = \frac{2 \times 450}{3} = 300 \text{ N.} \quad \blacktriangleleft$$

Another way: ^(less physical) Using (*) above,

$$\underline{e}_{AD} \cdot (\underline{r}_{AE} \times \underline{T}) = P \underline{e}_{AD} \cdot (\underline{r}_{AC} \times \underline{j})$$

$$\Rightarrow \underline{T} \cdot (\underline{e}_{AD} \times \underline{r}_{AE}) = P \left(\frac{2}{3}\underline{i} + \frac{2}{3}\underline{j} - \frac{1}{3}\underline{k} \right) \cdot \left[(4\underline{i} + 4\underline{j}) \times \underline{j} \right]$$

$$\underline{T} \cdot \left[\frac{4}{3}\underline{i} - \frac{2}{3}\underline{j} + \left(\frac{8}{3} - \frac{4}{3} \right) \underline{k} \right] = -\frac{4}{3}P \quad \rightarrow (**)$$

If T is minimum then \underline{T} should lie along $(\underline{e}_{AD} \times \underline{r}_{AE})$

$$\text{ie } \underline{T} = T_{\min} (4/3\underline{i} - 2/3\underline{j} + 4/3\underline{k}) / \sqrt{\frac{36}{9}} = T_{\min} \left(\frac{2}{3}\underline{i} - \frac{1}{3}\underline{j} + \frac{2}{3}\underline{k} \right)$$

$$(**) \Rightarrow T_{\min} \left(\frac{8}{9} + \frac{2}{9} + \frac{8}{9} \right) = -\frac{4}{3}(450) \Rightarrow T_{\min} = -\frac{4(450)(3)}{18} = -300$$

So T_{\min} is magnitude 300 N in direction $\left(-\frac{2}{3}\underline{i} + \frac{1}{3}\underline{j} - \frac{2}{3}\underline{k} \right)$

The rest follows from first method. Same as $\underline{e}_{EG'}$ of first method.

Method 3 — (too cumbersome but straightforward) (5)

$$\underline{I} = T((x+2)\underline{i} + y\underline{j} - 2\underline{k}) \quad \text{where } (x,y) \in G'$$

$$\underline{e}_{AD} \cdot (\underline{v}_{AE} \times \underline{I}) = T \frac{\left(-\frac{2}{3}y - \frac{8}{3} + \frac{4}{3}(x+2)\right)}{\sqrt{(x+2)^2 + y^2 + 4}} = T f(x,y)$$

So we wish to find max value of $f(x,y)$, then T will be minimum. So $\frac{\partial f(x,y)}{\partial x} = 0$, $\frac{\partial f(x,y)}{\partial y} = 0$, get complicated equations (two of them) in terms of x, y & solve for x, y . (Wght work^{out} in practical situation) may not like test, exam