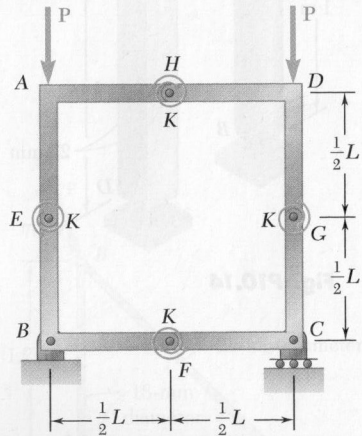
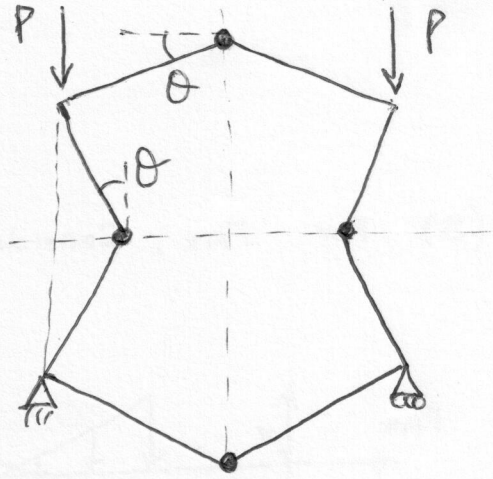
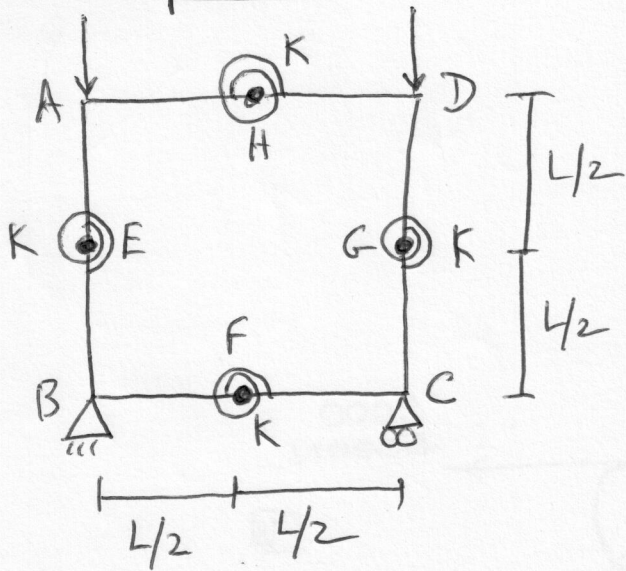


A frame consists of four L-shaped members connected by four torsional springs, each of constant  $K$ . Knowing that equal loads  $\mathbf{P}$  are applied at points  $A$  and  $D$  as shown, determine the critical value  $P_{cr}$  of the loads applied to the frame.



# Example 1

(1)

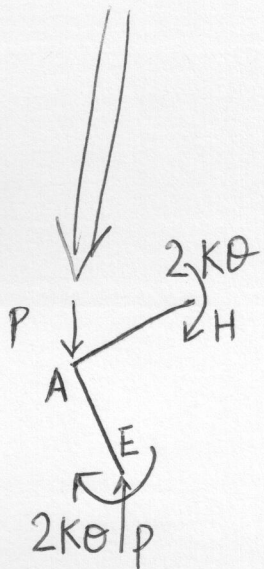


$\Rightarrow$  Symmetry  $\Rightarrow W=0, \Rightarrow R=P.$

$\Rightarrow$  External equilibrium (for full structure)  
 $U=0, V=P.$

$\Rightarrow \sum M_B = 0 \Rightarrow Q=T=0$   
 Half FBD (HAEBF)

Thus from quarter FBD (HAE),  $S=Q=0.$



$$\sum M_A = 0 = P\left(\frac{L}{2}\theta\right) = 2(2K\theta) \Rightarrow \boxed{P_{cr} = \frac{8K}{L}}$$

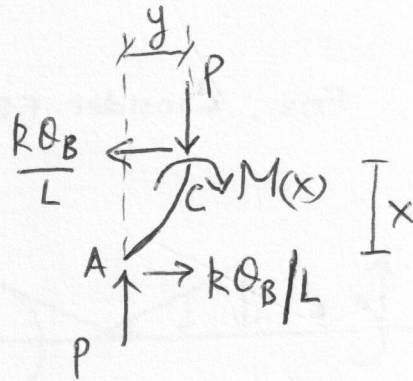
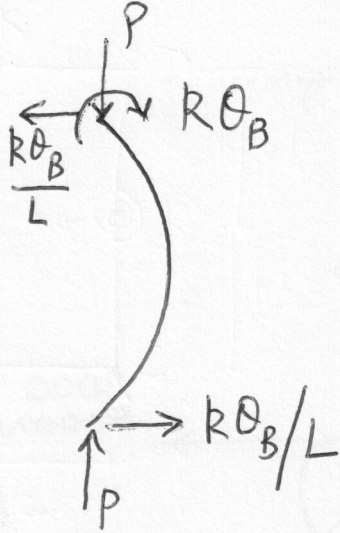
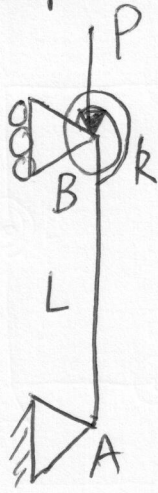
for  $\theta \neq 0.$

By Potential energy,  $4\left(\frac{1}{2}K(2\theta)^2\right) - 2\left[P\left[L - 2 \cdot \frac{L}{2} \cos\theta\right]\right] = V$

$$\frac{\partial V}{\partial \theta} = 0 \Rightarrow 16K\theta - P2L \sin\theta \stackrel{\approx \theta}{\approx}$$

$$\Rightarrow P_{cr} = \frac{8K}{L}$$

Example 2 Simply supported with partial restrain - column. (2)<sup>2</sup>



$$\sum M_c = 0 \Rightarrow Py + M(x) - \frac{R\theta_B}{L} x = 0$$

$$Py + EI y'' - \frac{R\theta_B}{L} x = 0, \text{ let } K^2 = \frac{P}{EI}$$

$$y = C_1 \cos Kx + C_2 \sin Kx + \frac{R\theta_B}{PL} x = 0$$

BC'S

$$x=0, y=0 \rightarrow C_1 = 0$$

$$x=L, y=0 \rightarrow C_2 \sin KL + \frac{R\theta_B}{PL} L = 0.$$

$$x=L, y' = -\theta_B \rightarrow C_2 K \cos KL + \frac{R\theta_B}{PL} = -\theta_B$$

$$\begin{bmatrix} \sin KL & R/P \\ K \cos KL & 1 + \frac{R}{PL} \end{bmatrix} \begin{Bmatrix} C_2 \\ \theta_B \end{Bmatrix} = 0 \rightarrow \text{eVP}$$

$$\det [ ] = 0 \text{ for non-zero } \{C_2 \ \theta_B\}^T.$$

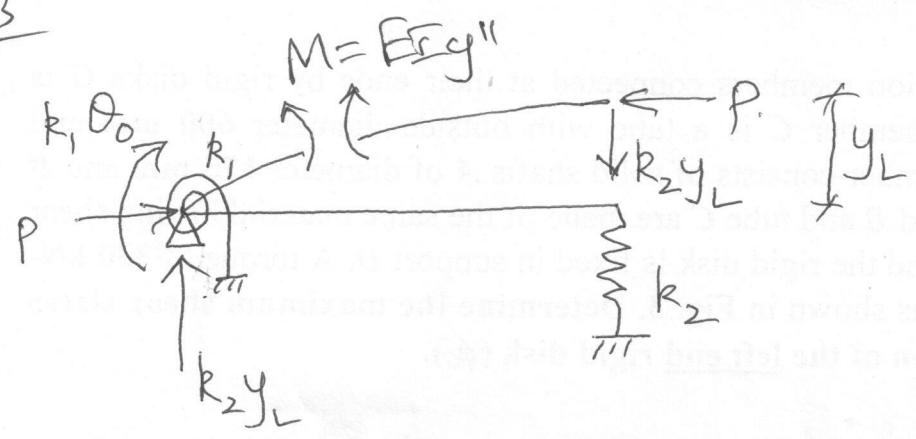
$$\tan KL = \frac{KR}{P} \left(1 + \frac{R}{PL}\right)^{-1} = \frac{KRL}{PL + R} = KL \left( \frac{R}{K^2 EI L + R} \right)$$

$$\tan KL = KL \left( \frac{1}{\frac{EI}{R} K^2 L + 1} \right) \rightarrow \text{solve numerically}$$

As  $R \rightarrow \infty$  it approaches fixed-pinned/roller (see Case III of before) ← Column.



P3



$$P y + EI y'' - k_2 y_L x - k_1 \theta_0 = 0, \quad k^2 = \frac{P}{EI}$$

$$y(x) = A \cos kx + B \sin kx + \frac{k_1 \theta_0}{P} + \frac{k_2 y_L}{P} x$$

$$\begin{matrix} y(0) = 0 & \longrightarrow & \left[ \begin{array}{cccc} 1 & 0 & 1 & 0 \\ \cos kL & \sin kL & 1 & (-\frac{P+L}{k_2}) \\ 0 & k & -P/k_1 & 1 \\ 0 & 0 & P & (PL - \frac{P^2}{k_2}) \end{array} \right] \begin{Bmatrix} A \\ B \\ k_1 \theta_0 / P \\ k_2 y_L / P \end{Bmatrix} \\ y(L) = y_L & \longrightarrow & \\ y'(0) = \theta_0 & \longrightarrow & \\ k_1 \theta_0 + k_2 y_L L - P y_L = 0 & \longrightarrow & \end{matrix}$$

det = 0 or solve simultaneously  $\Rightarrow = 0$

$$A = -k_1 \theta_0 / P; \quad \frac{k_2 y_L}{P} = -\frac{P}{(PL - P^2/k_2)} k_1 \theta_0 / P$$

$$B = \frac{1}{k} \left[ \frac{P}{k_1} + \frac{1}{L - P/k_2} \right] \frac{k_1 \theta_0}{P}$$

So characteristic equation is,

$$\frac{k_1 \theta_0}{P} \left[ -\cos kL + \sin kL \frac{1}{k} \left[ \frac{k^2 EI}{k_1} + \frac{1}{L - k^2 EI/k_2} \right] + 1 - \left[ \frac{-k^2 EI + L}{k_2} \right] \left[ \frac{1}{L - \frac{k^2 EI}{k_2}} \right] \right] = 0$$

For  $k_1 \rightarrow \infty, k_2 \rightarrow \infty$ , ie  $\Delta \longleftarrow P$ , get  $\tan kL = kL$

For  $k_1 \rightarrow 0, k_2 \rightarrow \infty$ , ie  $\Delta \longleftarrow P$ , get  $\tan kL = 0, kL = n\pi$

For  $k_1 \rightarrow \infty, k_2 \rightarrow 0$ , ie  $\Delta \longleftarrow P$ , get  $\tan kL \rightarrow \infty, kL = (2n+1)\frac{\pi}{2}, n=0,1,2,\dots$