

**Instructions:**

1. Attempt all questions.
2. All questions carry equal weight.
3. Make suitable assumptions, if necessary, and state the same clearly.

Q. 1. For the frame loaded as shown in **Fig. 1**, the deflections were found as  $\theta_B = 0.2041 \times 10^{-2}$  rad (clockwise),  $\theta_C = 0.5174 \times 10^{-3}$  rad (counter-clockwise),  $\theta_D = 0.2824 \times 10^{-4}$  rad (clockwise),  $\Delta_B = 0.8633 \times 10^{-2}$  m ( $\rightarrow$ ),  $\Delta_D = 0.1357 \times 10^{-1}$  m ( $\rightarrow$ ). Using **Slope Deflection Method**, find **ALL reactions** at joint **A**. Joints **B** and **D** are at the same horizontal level. Member lengths are shown against each member.  $EI = 2 \times 10^{14}$  N.mm<sup>2</sup> for all members.

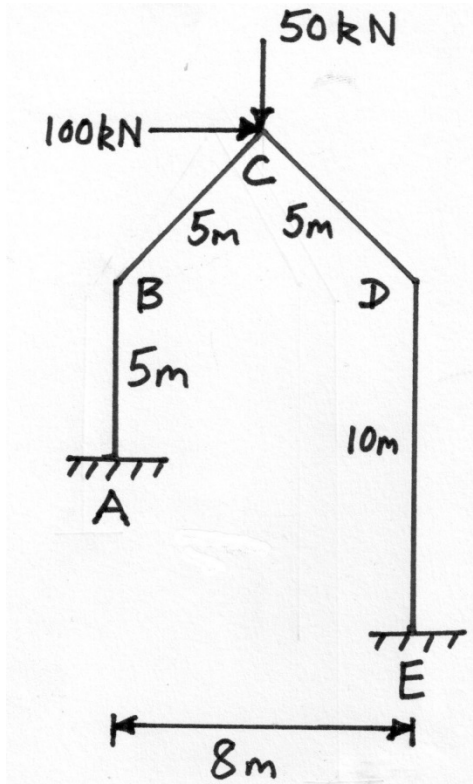


Fig. 1

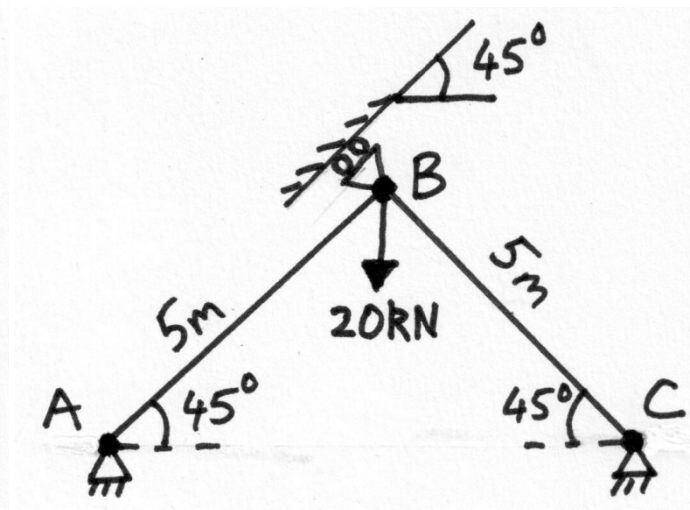


Fig.2

Q. 2. Using **Matrix Stiffness Method**, determine the **displacement of joint B** of the two-member plane truss shown in **Fig. 2**. Joint **B** is an inclined roller support.  $EA = 8 \times 10^6$  N for all members.

- Q. 3 Joint displacements due to loads  $V$  and  $Q$  applied to the simply-supported plane truss in Fig. 3 are given in Table 1. **Determine the loads  $V$  and  $Q$  that cause these displacements.**  $EA = 8 \times 10^6$  N for all members.

Table 1.

Joint	X - displacement (m)	Y - displacement (m)
1	0.00000	0.00000
2	0.07294	0.00000
3	0.01425	-0.10700
4	0.06919	-0.08835
5	0.03338	-0.16080
6	0.05494	-0.15450
7	0.05046	-0.16230
8	0.03452	-0.15460
9	0.06883	-0.10670
10	0.02252	-0.08540
11	0.08083	0.00000
12	0.02252	0.00000

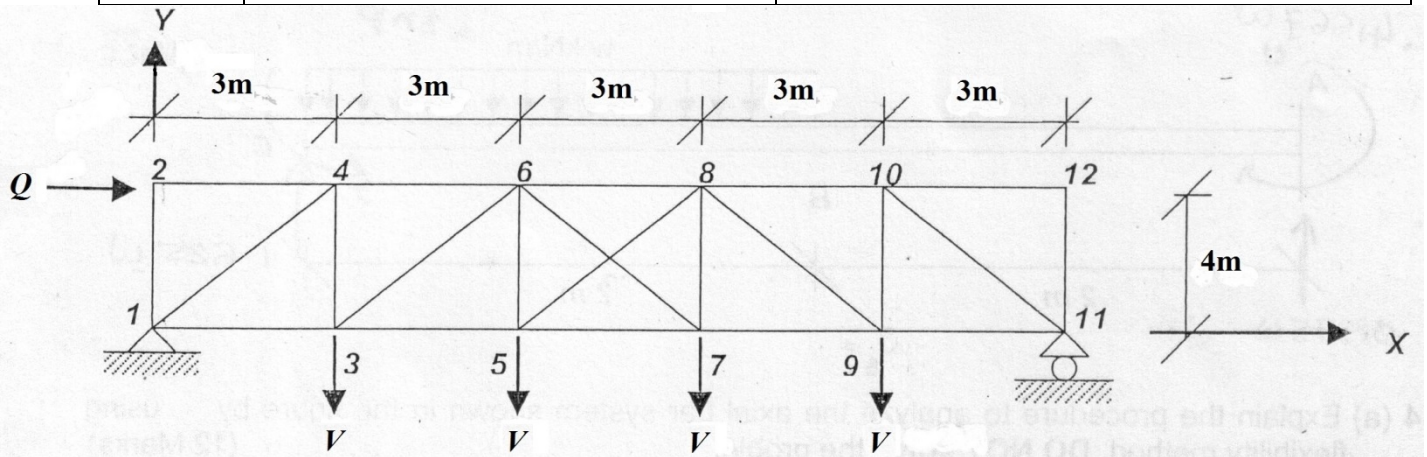


Fig. 3

- Q. 4 The space truss in Fig. 4 comprises three members  $AD$ ,  $BD$ ,  $CD$ , each with length 1 m. Coordinates (in m) are:  $A = \left(0, 0, \frac{1}{\sqrt{3}}\right)$ ,  $B = \left(-\frac{1}{2}, 0, -\frac{1}{2\sqrt{3}}\right)$ ,  $C = \left(\frac{1}{2}, 0, -\frac{1}{2\sqrt{3}}\right)$ ,

$D = \left(0, \sqrt{\frac{2}{3}}, 0\right)$ . Supports  $A$ ,  $B$ ,  $C$ , are ball and sockets. Member  $CD$  is heated to  $70^\circ\text{C}$

above ambient temperature. Determine displacements at joint  $D$ . Use  $EA = 8 \times 10^6$  N for all members, and  $\alpha = 5 \times 10^{-6} / ^\circ\text{C}$  for  $CD$ .

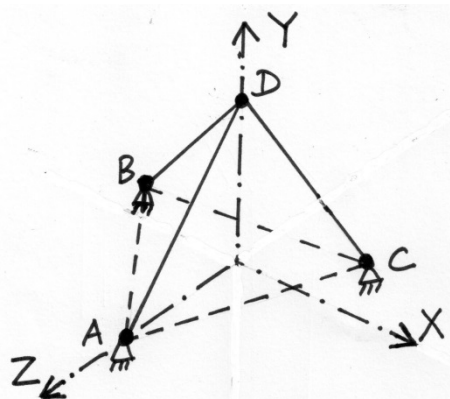


Fig. 4

Q1  $M_{AB} = \frac{2 \times 10^4}{5 \times 10^3} \left( 2 \times 0.2041 \times 10^{-2} - 6 \times \frac{0.8633 \times 10^{-2}}{5} \right) = -2.51104 \times 10^8 \text{ N.mmm}$   
 $= -2.511 \times 10^2 \text{ kN.m}$

$M_{BA} = \frac{2 \times 10^4}{5 \times 10^3} \left( 4 \times 0.2041 \times 10^{-2} - 6 \times \frac{0.8633 \times 10^{-2}}{5} \right) = -8.7824 \times 10^7 \text{ N.mmm}$

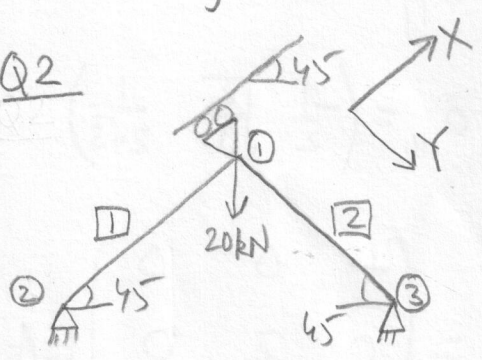
$A_x = \frac{M_{AB} + M_{BA}}{5 \times 10^3} = -6.77856 \times 10^4 \text{ N} = -67.79 \text{ kN} (\leftarrow)$

$M_{ED} = \frac{2 \times 10^4}{10 \times 10^3} \left( 2 \times 0.2824 \times 10^{-4} - 6 \times \frac{0.1357 \times 10^{-1}}{10} \right) = -1.617104 \times 10^8$

$A_y = \frac{(+M_{AB} - M_{ED} - 100 \times 10^3 \times 13 \times 10^3 + 50 \times 10^3 \times 4 \times 10^3 - A_x \times 5 \times 10^3)}{8 \times 10^3}$

$A_y = -43532.2 \text{ N} = -43.53 \text{ kN} (\downarrow)$

Q2



$a_{12} = [1 \ 0], a_{13} = [0 \ -1]$

$K_{II} = \frac{EA}{L} \begin{bmatrix} 1 & 0 & & \\ 0 & 0 & & \\ & & 1 & 0 \\ & & 0 & 0 \end{bmatrix}$

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$K_{II} = \left[ \frac{EA}{L} \right]_1; P_I = \left[ -\frac{20 \times 10^3}{\sqrt{2}} \right]_1; \Delta_I = K_{II}^{-1} P_I = -8.8388 \text{ mm.}$

Q3  $F_{24} = k_{22}^4 a_{24} \Delta_2 + k_{24} a_{42} \Delta_4 = \frac{EA}{3} \left( [-1 \ 0] \begin{bmatrix} 0.07294 \\ 0 \end{bmatrix} + [1 \ 0] \begin{bmatrix} 0.06919 \\ -0.08835 \end{bmatrix} \right) = -10000 \text{ N}$

Joint equl (method of joints) at joint 2  $\Rightarrow Q + F_{24} = 0 \Rightarrow Q = 10000 \text{ N.}$

$F_{34} = \frac{EA}{4} \left( [0 \ -1] \begin{bmatrix} 0.01425 \\ -0.10700 \end{bmatrix} + [0 \ 1] \begin{bmatrix} 0.06919 \\ -0.08835 \end{bmatrix} \right) = 37300 \text{ N}$

$F_{36} = \frac{EA}{5} \left( [-0.6 \ -0.8] \begin{bmatrix} 0.01425 \\ -0.10700 \end{bmatrix} + [0.6 \ 0.8] \begin{bmatrix} 0.05494 \\ -0.15450 \end{bmatrix} \right) = -21737.6 \text{ N}$

Joint equl at jlt. 3  $\Rightarrow V = F_{34} + F_{36} \times 0.8 = 19909.92 \text{ N}$

$F_{56} = \frac{EA}{4} \left( [0 \ -1] \begin{bmatrix} 0.03338 \\ -0.16080 \end{bmatrix} + [0 \ 1] \begin{bmatrix} 0.05494 \\ -0.15450 \end{bmatrix} \right) = 12600 \text{ N}$

Q4  $F_{58} = \frac{EA}{5} \left( [-0.6 \ -0.8] \begin{bmatrix} 0.03338 \\ -0.16080 \end{bmatrix} + [0.6 \ 0.8] \begin{bmatrix} 0.03452 \\ -0.15460 \end{bmatrix} \right) = 9030.4$

Joint equl. at jlt. 5  $\Rightarrow V = F_{56} + F_{58} \times 0.8 = 19824.32 \text{ N}$

$$F_{78} = \frac{EA}{4} \left( [0 \ -1] \begin{bmatrix} 0.05046 \\ -0.16230 \end{bmatrix} + [0 \ 1] \begin{bmatrix} 0.03452 \\ -0.15460 \end{bmatrix} \right) = 15400 \text{ N} \quad (2)$$

$$F_{76} = \frac{EA}{5} \left( [0.6 \ -0.8] \begin{bmatrix} 0.05046 \\ -0.16230 \end{bmatrix} + [-0.6 \ 0.8] \begin{bmatrix} 0.05494 \\ -0.15450 \end{bmatrix} \right) = 5683.2 \text{ N}$$

Joint equil at jt (7)  $\Rightarrow V = F_{78} + F_{76} \times 0.8 = \underline{19946.56 \text{ N}}$

$$F_{9,10} = \frac{EA}{4} \left( [0 \ -1] \begin{bmatrix} 0.06883 \\ -0.10670 \end{bmatrix} + [0 \ 1] \begin{bmatrix} 0.02252 \\ -0.08540 \end{bmatrix} \right) = 42600 \text{ N}$$

$$F_{98} = \frac{EA}{5} \left( [0.6 \ -0.8] \begin{bmatrix} 0.06883 \\ -0.10670 \end{bmatrix} + [-0.6 \ 0.8] \begin{bmatrix} 0.03452 \\ -0.15460 \end{bmatrix} \right) = -28374 \text{ N}$$

Joint equil at jt (9)  $\Rightarrow V = F_{9,10} + F_{98} \times 0.8 = \underline{19900.8 \text{ N}}$

P4 D  $\rightarrow$  ①, A  $\rightarrow$  ②, B  $\rightarrow$  ③, C  $\rightarrow$  ④ is jt. numbering.

$$K_{II} = \sum_{j=2,3,4} [K]_{ij}^j = \sum a_{ij}^T [K]_{ij}^j a_{ij} = \frac{EA}{L} \sum a_{ij}^T a_{ij}$$

$$a_{12} = \left( 0, \sqrt{\frac{2}{3}}, -\frac{1}{\sqrt{3}} \right); \quad a_{13} = \left( \frac{1}{2}, \sqrt{\frac{2}{3}}, \frac{1}{2\sqrt{3}} \right); \quad a_{14} = \left( -\frac{1}{2}, \sqrt{\frac{2}{3}}, \frac{1}{2\sqrt{3}} \right)$$

$$K_{II} = EA \begin{bmatrix} 0 + \frac{1}{4} + \frac{1}{4} & 0 + \frac{1}{\sqrt{6}} - \frac{1}{\sqrt{6}} & 0 + \frac{1}{4\sqrt{3}} - \frac{1}{4\sqrt{3}} \\ \frac{2}{3} + \frac{2}{3} + \frac{2}{3} & -\frac{\sqrt{2}}{3} + \frac{1}{\sqrt{18}} + \frac{1}{\sqrt{18}} & \frac{1}{3} + \frac{1}{12} + \frac{1}{12} \\ \text{symm} & & \end{bmatrix} = \begin{bmatrix} \frac{1}{2} & 0 & 0 \\ 0 & 2 & 0 \\ 0 & 0 & \frac{1}{2} \end{bmatrix} EA$$

$$P_I = P/a - P_{se} = -a_{14}^T F_{14}^{sf} = - \begin{bmatrix} -\frac{1}{2} & \sqrt{\frac{2}{3}} & \frac{1}{2\sqrt{3}} \end{bmatrix}^T \left( R_{11} \begin{pmatrix} 4 \\ -5 \\ 14 \end{pmatrix} + R_{14} \begin{pmatrix} -5 \\ 4 \\ 1 \end{pmatrix} \right)$$

$$= - \begin{bmatrix} -\frac{1}{2} & \sqrt{\frac{2}{3}} & \frac{1}{2\sqrt{3}} \end{bmatrix}^T \cdot (-35 \times 10^{-5} \cdot EA)$$

$$P_I = EA \times 10^{-5} \begin{bmatrix} -\frac{35}{2} & 35\sqrt{\frac{2}{3}} & \frac{35}{2\sqrt{3}} \end{bmatrix}^T$$

$$\Delta_I = 10^{-5} \begin{bmatrix} -35 & \frac{35}{\sqrt{6}} & \frac{35}{\sqrt{3}} \end{bmatrix}^T \text{ m} = [-0.35 \ 0.1429 \ 0.2021] \text{ mm}$$

