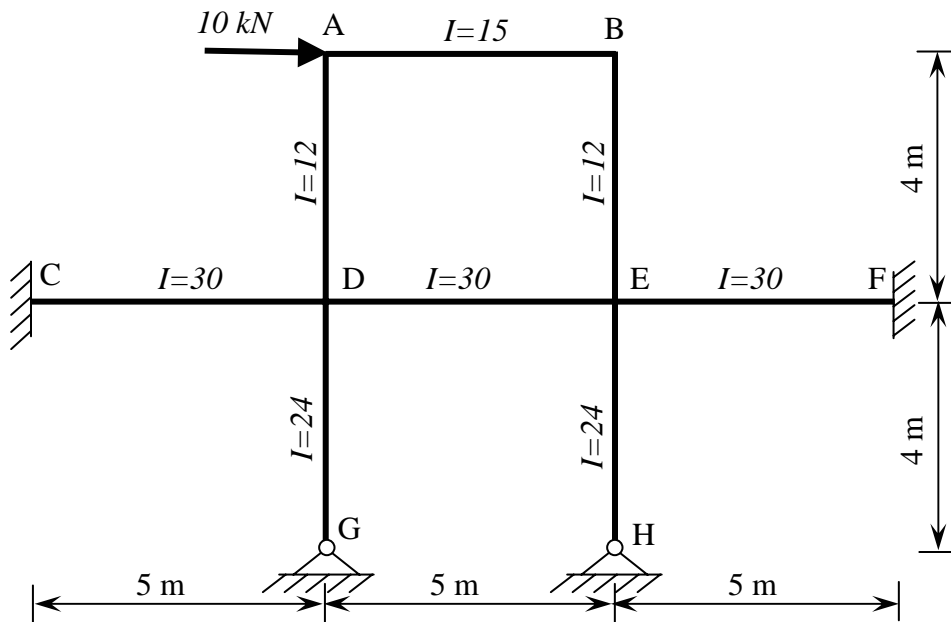
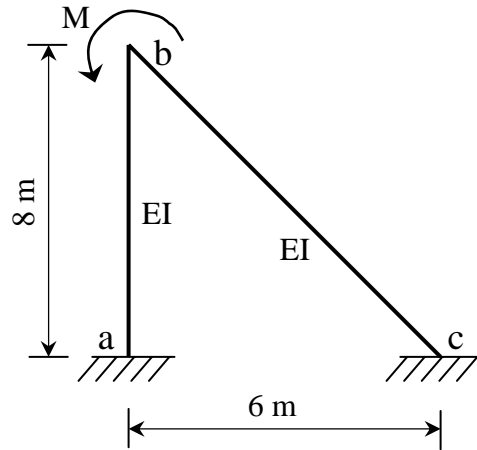
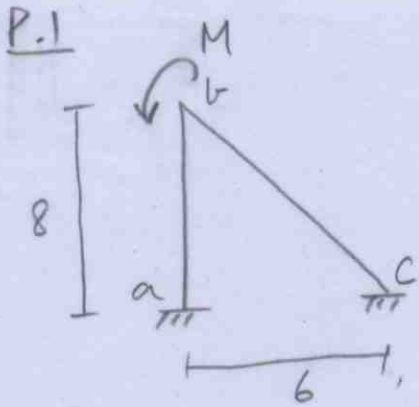


Use moment distribution method. Draw BMD, SFD, and deflected shape.

P1



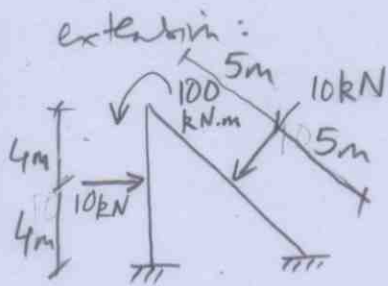
P2



jt	a	b	b	c
mem end	ab	ba	bc	cb
rel stiff	R	R	0.8R	0.8R
df	0	0.555	0.444	0
fem	0	0	0	0
convg BM	-0.277 M	-0.555 M	-0.444 M	-0.222 M

$R = \frac{EI}{8}$

→ here the distribution is such that an imbalance of M is maintained at jt. b.



No sway possible in this problem.

jt	a	b	b	c
mem end	ab	ba	bc	cb
df	0	0.555	0.444	0
fem	-10	10	-12.5	12.5
	-27.06	(1.3875 -55.5)	(1.11 -44.4)	-21.65
	-37.06	-44.11	-55.8	-9.15

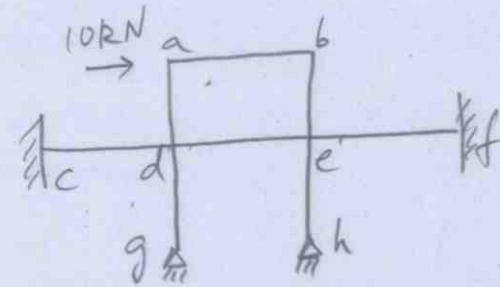
P2

TUTORIAL-3

< Result matches P2, tutorial 2, done by slope-defl >

jt	a	a	d	d	d	d	c	
mem end	ab	ad	da	de	dg	dc	cd	
rel stiff	0.5	0.5	0.5	1	1	1	1	*k
mod stiff	0.75	0.5	0.5	1.5	0.75		1	*k
df	0.6	0.4	0.133333	0.4	0.2	0.266667		0
fem		-100	-100					
	60	40	13.33333	40	20	26.66667		
		6.666667	20				13.33333	
	-4	-2.666667	-2.666667	-8	-4	-5.333333		
		-1.333333	-1.333333				-2.666667	
	0.8	0.533333	0.177778	0.533333	0.266667	0.355556		
		0.088889	0.266667				0.177778	
	-0.053333	-0.035556	-0.035556	-0.106667	-0.053333	-0.071111		
convg BM	56.74667	-56.74667	-70.25778	32.42667	16.21333	21.61778	10.84444	
dx	31.75111	from momt equil of da, left +ve						
ex	31.75111	from antisymm, or momt equil of be, left +ve						
r	63.50222	right +ve						
scaled BM	8.93617	-8.93617	-11.06383	5.106383	2.553191	3.404255	1.707727	

No no-sway part of soln here.  
4\*e\*30/5=k



Relative stiffnesses

$$K_{cd} = \frac{4E \cdot 30}{5} = K = K_{dc} = K_{de}$$

$$K_{ab} = K_{ba} = \frac{4E \cdot 15}{5} = \frac{K}{2}$$

$$K_{ad} = K_{da} = \frac{4E \cdot 12}{4} = \frac{K}{2}$$

$$K_{dg} = K_{gd} = \frac{4E \cdot 24}{4} = K$$

Modified stiffnesses

Use modifications for pinned ends g, h, and antisymmetry of members ab, de.

$$K'_{ab} = \frac{K}{2} \cdot \frac{6}{4} = 0.75K$$

$$K'_{dg} = K \cdot \frac{3}{4} = 0.75K$$

$$K'_{de} = K \cdot \frac{6}{4} = 1.5K$$

- (i) No no-sway part of soln in this problem, ie only sway part.
- (ii) Simultaneous distribution at all jts followed by simultaneous c.o. to all jts (ie method-2).
- (iii) Only half structure considered since antisymmetric modified stiffnesses used.
- (iv) Jt. g excluded (zero BM). If dg was loaded then modified FEM (RHS table, Hibbeler) can be used.
- (iv) No distribution at c and no c.o. from c.
- (vi)  $\Sigma M_a = 0$ , get dx. Then  $dx + ex = 10$ . Scale dx, ex, to satisfy this, and then use this scaling to get final BM's