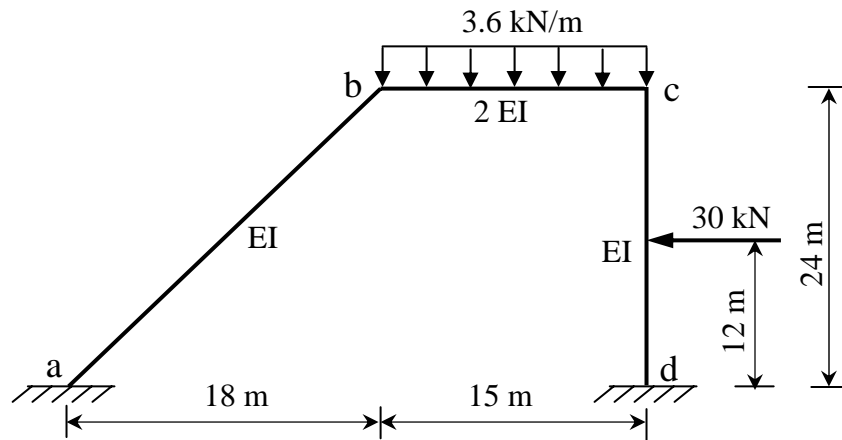


Department of Civil Engineering, IIT Bombay
Structural Mechanics –II

CE317

Tutorial 6

Use stiffness method to find joint deflections, member end forces, and reactions. Compare with results obtained by slope deflection method and moment distribution method, which neglect axial deformations. Use $I/A=3000\text{mm}^2$



%Tutorial 6 solution

%g=A/I in m² for respective member

g12=1/3000*1e6; g23=1/3000*1e6; g34=1/3000*1e6;

%matrix multiplications in matlab

a12=[-0.6 0.8 0; -0.8 -0.6 0; 0 0 1]; a21=[0.6 -0.8 0; 0.8 0.6 0; 0 0 1];
a23=[-1 0 0; 0 -1 0; 0 0 1]; a32=[1 0 0; 0 1 0; 0 0 1]; a34=[0 -1 0; 1 0 0; 0 0 1];
a43=[0 1 0; -1 0 0; 0 0 1];

L1=30; L2=15; L3=24;

k112=1/L1*[g12 0 0; 0 12/L1² -6/L1; 0 -6/L1 4]; k221=k112;

k12=1/L1*[g12 0 0; 0 12/L1² -6/L1; 0 -6/L1 2]; k21=k12;

k223=2/L2*[g23 0 0; 0 12/L2² -6/L2; 0 -6/L2 4]; k332=k223;

k23=2/L2*[g23 0 0; 0 12/L2² -6/L2; 0 -6/L2 2]; k32=k23;

k334=1/L3*[g34 0 0; 0 12/L3² -6/L3; 0 -6/L3 4]; k443=k334;

k34=1/L3*[g34 0 0; 0 12/L3² -6/L3; 0 -6/L3 2]; k43=k34;

K11=a12'*k112*a12; K12=a12'*k12*a21; K21=K12';

K22=a21'*k221*a21 + a23'*k223*a23;

K33=a32'*k332*a32 + a34'*k334*a34;

K23=a23'*k23*a32; K32=K23';

K34=a34'*k34*a43; K43=K34'; K44=a43'*k443*a43;

K13=zeros(3,3); K14= zeros(3,3); K24= zeros(3,3); K31= zeros(3,3);
K41= zeros(3,3); K42= zeros(3,3);

%remove rows/cols 1,2,3,10,11,12 from K_Total

KII=[K22 K23; K32 K33];

%remove rows 3,4,5,6,7,8 and cols 1,2,3,10,11,12 from K_Total

KII_I=[K12 K13; K42 K43];

F12f=[0 ; 0 ; 0]; F21f=[0 ; 0 ; 0];

F23f=[0 ; 3.6*L2/2 ; -3.6*L2²/12];

F32f=[0 ; -3.6*L2/2 ; 3.6*L2^2/12];
F34f=[0 ; 30/2 ; -30*L3/8]; F43f=[0 ; -30/2 ; 30*L3/8];

P1e= a12'*F12f; P2e= a21'*F21f + a23'*F23f;
P3e=a32'*F32f+ a34'*F34f; P4e=a43'*F43f;
Pa=[0 0 0 0 0 0]';

Pe=[P1e' P2e' P3e' P4e']'; Petilde=[P2e' P3e']';
PI=Pa-Petilde; Pehat= [P1e' P4e']';
DeltaI=inv(KII)*PI

DeltaI =
606.8382
458.0569
82.3718
606.4830
2.3979
-24.9287

%reactions
P_II=KII_I*DeltaI+Pehat

P_II =
15.7861
-20.6961
0.4228
14.2139
-33.3039
81.6051

%member end forces
DeltaII=[0 0 0 0 0 0]';
Delta1= [DeltaII(1); DeltaII(2); DeltaII(3)];
Delta2= [DeltaI(1); DeltaI(2); DeltaI(3)];
Delta3= [DeltaI(4); DeltaI(5); DeltaI(6)];

$$\begin{aligned} \Delta_4 &= [\Delta_{II}(4); \Delta_{II}(5); \Delta_{II}(6)]; \\ F_{12} &= k_{112} * a_{12} * \Delta_1 + k_{12} * a_{21} * \Delta_2 + F_{12f} \\ F_{21} &= k_{21} * a_{12} * \Delta_1 + k_{221} * a_{21} * \Delta_2 + F_{21f} \\ F_{23} &= k_{223} * a_{23} * \Delta_2 + k_{23} * a_{32} * \Delta_3 + F_{23f} \\ F_{32} &= k_{23} * a_{23} * \Delta_2 + k_{332} * a_{32} * \Delta_3 + F_{32f} \\ F_{34} &= k_{334} * a_{34} * \Delta_3 + k_{34} * a_{43} * \Delta_4 + F_{34f} \\ F_{43} &= k_{43} * a_{34} * \Delta_3 + k_{443} * a_{43} * \Delta_4 + F_{43f} \end{aligned}$$

$$\begin{aligned} F_{12} &= \\ &-26.0286 \\ &-0.2112 \\ &0.4228 \end{aligned}$$

$$\begin{aligned} F_{21} &= \\ &-26.0286 \\ &-0.2112 \\ &5.9142 \end{aligned}$$

$$\begin{aligned} F_{23} &= \\ &-15.7861 \\ &20.6961 \\ &-5.9142 \end{aligned}$$

$$\begin{aligned} F_{32} &= \\ &-15.7861 \\ &-33.3039 \\ &100.4723 \end{aligned}$$

$$\begin{aligned} F_{34} &= \\ &-33.3039 \\ &15.7861 \\ &-100.4723 \end{aligned}$$

$$\begin{aligned} F_{43} &= \\ &-33.3039 \\ &-14.2139 \\ &81.6051 \end{aligned}$$