

→ The aim is to eliminate all  $v_i$ 's and  $e_i$ 's in favor of  $v$  &  $e$ .

<p>P-1.</p> $e = e_3 = e_1 + e_2 \rightarrow (d)$ $e_1 = e_4 \rightarrow (b)$ $v_2 = v_1 + v_4 \rightarrow (c)$ $v = v_3 + v_2 \rightarrow (d)$	$v_1 = k_1 e_1 \rightarrow (e)$ $v_2 = c_2 \dot{e}_2 \rightarrow (f)$ $v_3 = k_3 e_3 \rightarrow (g)$ $v_4 = c_4 \dot{e}_4 \rightarrow (h)$
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Using (d, f, g, a<sub>1</sub>, a<sub>2</sub>)

$$v = v_3 + v_2 = k_3 e_3 + c_2 \dot{e}_2 = k_3 e + c_2 (\dot{e} - \dot{e}_1) \rightarrow (1)$$

Using (a<sub>2</sub>, b, f, h, c, d) g, a<sub>1</sub>.

Also,  $\dot{e} = \dot{e}_1 + \dot{e}_2 = \frac{v_4}{c_4} + \frac{v_2}{c_2} = \frac{v_2 - v_1}{c_4} + \frac{v - v_3}{c_2}$

$$= \frac{v - v_3 - v_1}{c_4} + \frac{v - v_3}{c_2} = (v - \underbrace{v_3}_{=k_3 e}) \left( \frac{1}{c_4} + \frac{1}{c_2} \right) - \frac{v_1}{c_4}$$

$$\dot{e} = (v - k_3 e) \left( \frac{1}{c_4} + \frac{1}{c_2} \right) - \frac{v_1}{c_4} \rightarrow (2)$$

Substitute (2), (e) in (1):

$$v = k_3 e + c_2 \left( \dot{e} - \frac{v_1}{c_4} \right) = k_3 e + c_2 \left( \dot{e} - \frac{1}{k_1} \left\{ c_4 \left[ (v - k_3 e) \left( \frac{c_2 + c_4}{c_2 c_4} \right) - \dot{e} \right] \right\} \right)$$

$$= k_3 e + c_2 \left( \dot{e} + \frac{c_4}{k_1} \ddot{e} - \frac{c_4}{k_1} \left( \frac{c_2 + c_4}{c_2 c_4} \right) \dot{v} + \frac{c_4}{k_1} k_3 \left( \frac{c_2 + c_4}{c_2 c_4} \right) \dot{e} \right)$$

$$v + \left( \frac{c_2 + c_4}{k_1} \right) \dot{v} = k_3 e + \left[ c_2 + \frac{k_3}{k_1} (c_2 + c_4) \right] \dot{e} + \left( \frac{c_2 c_4}{k_1} \right) \ddot{e}$$

Alternative - I



We have,  $v_v = v_1 + v_4$ ,  $e_v = e_1 = e_4$ ,  $v_1 = k_1 e_1$ ,  $v_4 = c_4 \dot{e}_4$

$$\Rightarrow v_v = k_1 e_v + c_4 \dot{e}_v$$

Also,  $v_v = v_2$ ,  $e = e_3 = e_v + e_2$ ,  $v = v_2 + v_3$ ,  $v_2 = c_2 \dot{e}_2$ ,  $v_3 = k_3 e_3$

$$\begin{aligned} \Rightarrow \dot{v} &= \dot{v}_2 + \dot{v}_3 = c_2 \ddot{e}_2 + k_3 \dot{e}_3 = c_2 (\ddot{e} - \ddot{e}_v) + k_3 \dot{e} \\ &= c_2 \left( \ddot{e} - \frac{1}{c_4} [\dot{v}_v - k_1 \dot{e}_v] \right) + k_3 \dot{e} = \\ &= c_2 \left( \ddot{e} - \frac{1}{c_4} [\dot{v}_2 - k_1 (\dot{e} - \dot{e}_2)] \right) + k_3 \dot{e} = c_2 \left( \ddot{e} - \frac{1}{c_4} [\dot{v} - \dot{v}_3 - k_1 (\dot{e} - \frac{\sigma}{c_2})] \right) + k_3 \dot{e} \\ &= c_2 \left( \ddot{e} - \frac{1}{c_4} [\dot{v} - k_3 \dot{e}_3 - k_1 (\dot{e} - \frac{\sigma - \sqrt{3}}{c_2})] \right) + k_3 \dot{e} \\ &= c_2 \left( \ddot{e} - \frac{1}{c_4} [\dot{v} - k_3 \dot{e} - k_1 (\dot{e} - \frac{\sigma - k_3 e_3}{c_2})] \right) + k_3 \dot{e} \\ &= c_2 \ddot{e} - \frac{c_2}{c_4} \dot{v} + \frac{c_2 k_3}{c_4} \dot{e} + \frac{c_2 k_1}{c_4} \dot{e} - \frac{c_2 k_1}{c_4} \frac{\sigma}{c_2} + \frac{c_2 k_1 k_3}{c_4} \frac{e}{c_2} + k_3 \dot{e} \end{aligned}$$

$$\Rightarrow \sigma + \left( \frac{c_2 + c_4}{c_4} \right) \left( \frac{c_4}{k_1} \right) \dot{v} = \frac{c_2 c_4}{k_1} \ddot{e} + \left( \frac{c_2 k_3}{k_1} + c_2 + c_4 \frac{k_3}{k_1} \right) \dot{e} + k_3 e$$

checks out with previous result.  $\leftarrow$

Alternative - II

Use (a-h) but in L.T. (Laplace transform domain). Then eliminate  $E_i, \Sigma_i$  in favor of  $E$  &  $\Sigma$ .

Let  $\mathcal{L}(v_i) = \Sigma_i(s), \mathcal{L}(e_i) = E_i(s)$ .

$$\begin{aligned} \Sigma &= \Sigma_3 + \Sigma_2 = \Sigma_3 + \Sigma_1 + \Sigma_4 = k_3 E_3 + k_1 E_1 + s c_4 E_4 \\ &= k_3 E + k_1 (E - E_2) + s c_4 (E - E_2) \\ &= (k_3 + k_1) E + s c_4 E - (k_1 + s c_4) E_2 \\ &= (k_3 + k_1) E + s c_4 E - (k_1 + s c_4) \frac{\Sigma_{12}}{s c_2} \\ &= (k_3 + k_1) E + s c_4 E - (k_1 + s c_4) \frac{(\Sigma_1 - \Sigma_{13})}{s c_2} \xrightarrow{k_3 E_3} E \end{aligned}$$

- $E_1 + E_2 = E \checkmark$
- $E_3 = E \checkmark$
- $E_1 - E_3 = 0 \checkmark$
- $\Sigma_1 + \Sigma_4 - \Sigma_2 = 0 \checkmark$
- $\Sigma_2 + \Sigma_4 - \Sigma_1 = 0$
- $\Sigma_1 - k_1 E_1 = 0 \checkmark$
- $\Sigma_2 - s c_2 E_2 = 0 \checkmark$
- $\Sigma_3 - k_3 E_3 = 0 \checkmark$
- $\Sigma_4 - s c_4 E_4 = 0 \checkmark$

$$\Rightarrow s c_2 \Sigma = s c_2 (k_3 + k_1) E + s^2 c_2 c_4 E - (k_1 + s c_4) (\Sigma_1 - k_3 E)$$

$\mathcal{L}^{-1}$  gives,

$$c_2 \dot{\sigma} = c_2 (k_3 + k_1) \dot{e} + c_2 c_4 \ddot{e} - k_1 \sigma - c_4 \dot{\sigma} + k_1 k_3 e + c_4 k_3 \dot{e}$$

$$\Rightarrow \sigma + \frac{c_2 + c_4}{k_1} \dot{\sigma} = k_3 e + \left[ c_2 + \frac{k_3}{k_1} (c_2 + c_4) \right] \dot{e} + \frac{c_2 c_4}{k_1} \ddot{e} \rightarrow \text{same as before}$$

Creep response: Take Laplace transform with zero initial conditions. (3)

$$\Sigma (1+As) = E (B+Cs+Ds^2)$$

$$A = \frac{c_2+c_4}{k_1}, \quad B = k_3, \quad C = c_2 + \frac{k_3}{k_1}(c_2+c_4), \quad D = \frac{c_2 c_4}{k_1}$$

$$\text{Now } \Sigma = \frac{\sigma_0}{s}$$

$$\Rightarrow E = \sigma_0 \frac{1}{s} \frac{(1+As)}{(B+Cs+Ds^2)}$$

Examine roots of  $Ds^2 + Cs + B = 0$

$$\begin{aligned} C^2 - 4DB &= c_2^2 + \frac{k_3^2}{k_1^2} (c_2+c_4)^2 + 2c_2 \frac{k_3}{k_1} (c_2+c_4) - 4 \frac{k_3}{k_1} c_2 c_4 \\ &= c_2^2 + \frac{k_3^2}{k_1^2} (c_2-c_4)^2 + 2c_2 \frac{k_3}{k_1} (c_2-c_4) + 4 \frac{k_3^2}{k_1^2} c_2 c_4 \\ &= \left[ c_2 + \frac{k_3}{k_1} (c_2-c_4) \right]^2 + 4 \frac{k_3^2}{k_1^2} c_2 c_4 > 0 \end{aligned}$$

Thus  $\sqrt{C^2 - 4DB}$  is real and  $< C$ .

$\Rightarrow$  roots of  $Ds^2 + Cs + B = 0$  are real and negative.

i.e.,  $Ds^2 + Cs + B = D(s+a)(s+b)$  where  $(a, b) > 0$ .

$$\text{i.e., } a, b = \frac{-C \pm \sqrt{C^2 - 4BD}}{2D}$$

$\Rightarrow$  from L.T. tables,  $e(t) = \mathcal{L}^{-1} \left\{ \frac{\sigma_0}{D} \left( \frac{1}{s(s+a)(s+b)} + \frac{A}{(s+a)(s+b)} \right) \right\}$

$$e(t) = \frac{\sigma_0}{D} \left( \frac{1}{ab} \left[ 1 + \frac{1}{a-b} (b e^{-at} - a e^{-bt}) \right] + \frac{A}{b-a} \left[ \frac{e^{-at} - e^{-bt}}{a-b} \right] \right)$$

Creep response  $\rightarrow e(t) = \frac{\sigma_0}{D} \left( \frac{1}{ab} + \frac{1}{a-b} \left( e^{-at} \left[ \frac{1}{a} - A \right] + e^{-bt} \left[ A - \frac{1}{b} \right] \right) \right) \blacktriangleleft$

$$e(0^+) = \frac{\sigma_0}{D} \left( \frac{1}{ab} + \frac{1}{a-b} \left( \frac{1}{a} - A + A - \frac{1}{b} \right) \right) = \frac{\sigma_0}{D} \left( \frac{1}{ab} - \frac{1}{ab} \right) = 0$$

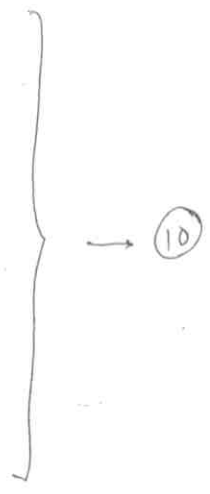
check: (i) Initial value theorem gives,

$$e(0) = \lim_{s \rightarrow \infty} s E(s) = \lim_{s \rightarrow \infty} \sigma_0 \frac{(1+As)}{(B+Cs+Ds^2)} = 0$$

(ii) Physically, we see that  $\because$  instantaneous strains in dashpots is zero, the instantaneous overall strain is zero.

P-2 Displacements :

$$\begin{aligned} \epsilon_x &= -\nu \frac{\sigma_z}{E} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} = \frac{du}{dx} \\ \epsilon_y &= -\nu \frac{\sigma_z}{E} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} = \frac{dv}{dy} \\ \epsilon_z &= \frac{\sigma_z}{E} = -\frac{x}{R_x} + \frac{y}{R_y} = \frac{dw}{dz} \\ \gamma_{xz} &= 0 = \frac{du}{dz} + \frac{dw}{dx} \\ \gamma_{yx} &= 0 = \frac{dv}{dy} + \frac{dw}{dx} \\ \gamma_{zy} &= 0 = \frac{dv}{dz} + \frac{dw}{dy} \end{aligned}$$



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$$(10c) \rightarrow w = -\frac{xz}{R_x} + \frac{yz}{R_y} + g(x,y) \rightarrow (i)$$

$$(10d, i) \rightarrow \frac{\partial u}{\partial z} = \frac{z}{R_x} - \frac{\partial g}{\partial x} \rightarrow u = \frac{z^2}{2R_x} - z \frac{\partial g}{\partial x} + f(x,y) \rightarrow (ii)$$

$$(10f, i) \rightarrow \frac{\partial v}{\partial z} = -\frac{z}{R_y} - \frac{\partial g}{\partial y} \rightarrow v = -\frac{z^2}{2R_y} - z \frac{\partial g}{\partial y} + h(x,y) \rightarrow (iii)$$

$$(10e, ii, iii) \rightarrow -2z \frac{\partial^2 g}{\partial x \partial y} + \frac{\partial f}{\partial y} + \frac{\partial h}{\partial x} = 0$$

$\xrightarrow{\text{fr. } g(x,y) \text{ only}}$

$$\Rightarrow \frac{\partial^2 g}{\partial x \partial y} = 0, \quad \frac{\partial f}{\partial y} = -\frac{\partial h}{\partial x} \rightarrow (iv, v)$$

$$(10a, ii, iii) \rightarrow -z \frac{\partial^2 g}{\partial x^2} + \frac{\partial f}{\partial x} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} \xrightarrow{\text{fr. } g(x,y) \text{ only}}$$

$$\Rightarrow \frac{\partial^2 g}{\partial x^2} = 0 \rightarrow (vi)$$

$$\frac{\partial f}{\partial x} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} \Rightarrow f = \frac{\nu x^2}{2R_x} - \frac{\nu xy}{R_y} + m(y) \rightarrow (vii)$$

$$(10b, ii, iii) \rightarrow -z \frac{\partial^2 g}{\partial y^2} + \frac{\partial h}{\partial y} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} \xrightarrow{\text{fr. } g(x,y) \text{ only}}$$

$$\Rightarrow \frac{\partial^2 g}{\partial y^2} = 0 \rightarrow (viii)$$

$$\frac{\partial h}{\partial y} = \frac{\nu x}{R_x} - \frac{\nu y}{R_y} \Rightarrow h = \frac{\nu xy}{R_x} - \frac{\nu y^2}{2R_y} + n(x) \rightarrow (ix)$$

$$(v, vii, ix) \rightarrow -\frac{\nu x}{R_y} + \frac{dn}{dy} = -\frac{\nu y}{R_x} - \frac{dm}{dx}$$

$\xrightarrow{\text{fr. } g}$

$$\Rightarrow m = -\frac{\nu y^2}{2R_x} + C_1 y + C_2$$

$$n = +\frac{\nu x^2}{2R_y} - C_1 x + C_3$$

Apply bc's  $u=v=w=0$  at  $(x,y,z) = (0,0,0)$ , and rotations  $(\frac{\partial w}{\partial x} - \frac{\partial u}{\partial z})$ ,  $(\frac{\partial w}{\partial y} - \frac{\partial v}{\partial z})$ ,  $(\frac{\partial u}{\partial y} - \frac{\partial v}{\partial x})$  are also zero at  $(x,y,z) = (0,0,0)$  (to get rid of P.B. matrices)

Now (iv, vi, viii) →  $g = c_4 x + c_5 y$

⇒  $u = \frac{z^2}{2R_x} - c_4 z + \frac{\nu}{2R_x} x^2 - \frac{\nu}{R_y} xy - \frac{\nu}{2R_x} y^2 + c_4 y + c_2$

$v = \frac{-z^2}{2R_y} - z c_5 + \frac{\nu}{R_x} xy - \frac{\nu}{2R_y} y^2 + \frac{\nu x^2}{2R_y} - c_4 x + c_5$

$w = -\frac{xz}{R_x} + \frac{yz}{R_y} + c_4 x + c_5 y$

BC'S ⇒  $c_1 = c_2 = c_3 = c_4 = c_5 = 0$  (could have got it by noting that const & linear terms in displ represent RB translation & rotation, so drop them).

⇒ 
$$\left. \begin{aligned} u &= \frac{1}{2R_x} [z^2 + \nu(x^2 - y^2)] - \frac{\nu}{R_y} xy \\ v &= \frac{1}{2R_y} [-z^2 + \nu(x^2 - y^2)] + \frac{\nu}{R_x} xy \\ w &= -\frac{xz}{R_x} + \frac{yz}{R_y} \end{aligned} \right\} \rightarrow (11)$$

# HW #5, P. 3. Solution.

## P. 3 Determination of Shear Center.

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Use (25) to determine  $(x_{CF}, y_{CF})$  as follows. So (25), (19), (22b), (23) yield,

$$\begin{aligned} x_{CF} w_y - y_{CF} w_x &= \int_A (x \tau_{yz} - y \tau_{xz}) dA \\ &= \int_A \left[ x \left( -\frac{\partial \phi}{\partial x} - g(x) - \frac{1}{2} E K_y y^2 \right) - y \left( \frac{\partial \phi}{\partial y} + f(y) - \frac{1}{2} E K_x x^2 \right) \right] dA \\ &= \int_A \left[ 2\phi + \frac{\partial}{\partial x} [-x\phi - xy f(y) + \frac{1}{6} E K_x x^3 y] - \frac{\partial}{\partial y} [y\phi + xy g(x) + \frac{1}{6} E K_y x y^3] \right] dA \\ &= \int_A 2\phi dA + \int_C [y\phi + xy g(x) + \frac{1}{6} E K_y x y^3] dx + \int_C [-x\phi - xy f(y) + \frac{1}{6} E K_x x^3 y] dy \\ &= \int_A 2\phi dA - \frac{1}{3} E \left[ K_y \int_C x y^3 dx + K_x \int_C x^3 y dy \right] \quad (\text{used (22b), (23)}) \\ &= \int_A (2\phi - E K_x x^2 y + E K_y x y^2) dA \end{aligned}$$

where  $\phi$  is determined from (20), (22b), (23), setting  $\alpha=0$ . Inserting (18) in the above & equating coefficients of  $w_x, w_y$  ( $\because$  they are independent), we obtain

$$x_{CF} = \frac{1}{w_y} \int_A \left[ 2w_y \phi_2 + \frac{I_{xy} w_y}{F} x^2 y + \frac{I_y w_y}{F} x y^2 \right] dA \quad \left. \vphantom{x_{CF}} \right\} \rightarrow (26)$$

$$\text{where } F = I_x I_y - I_{xy}^2$$

$$\text{and } y_{CF} = -\frac{1}{w_x} \int_A \left[ 2w_x \phi_1 - \frac{I_x w_x}{F} x^2 y - \frac{I_{xy} w_x}{F} x y^2 \right] dA$$

In the above we have used the fact that since (20) is linear in  $\phi$ , its solution is  $\phi = w_y \phi_2 + w_x \phi_1$  where  $\phi_2$  and  $\phi_1$  are solutions of (20), (22b), (23) with  $(w_y, w_x) = (1, 0)$  and  $(0, 1)$ , respectively. Thus  $\phi_1$  and  $\phi_2$  depend on the geometry of the cross-section <sup>only</sup> and consequently so does  $(x_{CF}, y_{CF})$ .