

Available online at www.sciencedirect.com





Composite Structures 84 (2008) 114-124

www.elsevier.com/locate/compstruct

# Application of polymer composites in civil construction: A general review

Sandeep S. Pendhari, Tarun Kant \*, Yogesh M. Desai

Department of Civil Engineering, Indian Institute of Technology Bombay, Powai, Mumbai 400 076, India

Available online 12 July 2007

#### Abstract

Different applications of fiber reinforced polymer composites (FRPCs) for external strengthening in civil construction are reviewed in this paper. Experimental as well as analytical and numerical research contributions have been focussed in the review. The main structural components such as beams, columns and beam-column joints, have been reviewed and structural behavior of each component is discussed briefly. Finally, general concluding remarks are made along with possible future directions of research. © 2007 Elsevier Ltd. All rights reserved.

Keywords: FRPC; CFRPC; GFRPC; AFRPC; Rehabilitation; Strengthening

# 1. Introduction

Advanced composite materials have found expanded use in aerospace, marine and automobile industries during the past few decades (1960 onwards) due to their good engineering properties such as high specific strength and stiffness, lower density, high fatigue endurance, high damping and low thermal coefficient (in fiber direction), etc. Recently, civil engineers and the construction industry have begun to realize potential of composites as strengthening material for many problems associated with the deterioration of infrastructures. Over the last decade, an increase in the application of FRPCs has been seen in construction industry because of their good engineering properties. Further, these are being considered as a replacement to the conventional steel in reinforced concrete structures due to continuing drop in the cost of FRPC materials. Various aspects of FRPC materials including guidelines for selection of polymer adhesives for concrete have been highlighted by ACI Committee-503 [1] and Uomoto et al. [2]. Issues related to selection of materials have also been discussed by Karbhari [3]. Einde et al. [4] and Bank et al. [5]

0263-8223/\$ - see front matter © 2007 Elsevier Ltd. All rights reserved. doi:10.1016/j.compstruct.2007.06.007

have presented a summary of applications of FRPC material in civil engineering whereas general design guidelines for FRPC application can be found in Bakht et al. [6], ACI Committee 440 [7] and Nanni [8].

Use of FRPC sheets for strengthening and rehabilitation of concrete structures has attracted considerable interest [9–12]. First applications of composites were in the form of rebars and structural shapes. Later, FRPC laminates were used for strengthening of concrete bridge girders by bonding them to the tension face of girder [13] as well as for retrofitting of concrete columns [14].

FRPC are available in the form of rods, grids, sheets and winding strands. Review of literature up to 1996 can be found in ACI Committee 440 [15]. Another general review on class of materials including FRPCs used in civil construction was presented by Bakis et al. [16]. They divided the whole review into structural shapes, internal reinforcement, externally bonded reinforcement, bridge, standards and codes. A review on shear strengthening of RC beams with FRPCs was done by Deniaud and Cheng [17], Bousselham and Chaallal [18]. Review related to the bond-slip model for FRPC sheet/plate bonded to concrete have been presented recently by Lu et al. [19] and review for upgrading of beam-column joints with FRPC can be found in Engindeniz et al. [20]. A large volume of literature

<sup>\*</sup> Corresponding author. Tel.: +91 22 2576 7310; fax: +91 22 2576 7302. *E-mail address:* tkant@iitb.ac.in (T. Kant).

now exists on applications of FRPCs in construction industry. However, literature up to July 2005 is considered here for general classification.

The main objectives of the paper are to classify the available literature (analytical/experimental) and to discuss the effects of various parameters such as fiber type, thickness, fiber angle, concrete strength, etc. Discussion is kept on a descriptive level and reader is advised to refer to the cited references for details of parameters and mathematical models.

#### 2. Repair and rehabilitation of structural elements

Majority of rehabilitation works consist of repair of old deteriorating structures, damage due to seismic activities and other natural hazards. Structural strengthening is also required because of degradation problems which may arise from environmental exposure, inadequate design, poor quality construction and a need to meet current design requirement. Therefore, structural repair and strengthening has received much attention over the past two decades throughout the world. Recent experimental and analytical research have demonstrated that the use of composite materials for retrofitting existing structural components is more cost-effective and requires less effort and time than the traditional means.

Historically, composites were first used as flexural strengthening materials for reinforced concrete (RC) bridges, as confining reinforcement for RC columns [21] and unreinforced masonry walls [14] against possible earthquake forces. Apart from strengthening of bridge girders, columns and walls, composites are also used in bridge decks and in cable stayed bridges. Strengthening of beams, columns and beam-column joints are discussed in the sequel.

### 2.1. Strengthening of RC beams by using FRPC

One of the most popular techniques for strengthening of RC beams has involved the use of external epoxy-bonded steel plates [22,23]. It has been demonstrated experimentally that flexural strength of a structural member can increase by about 15% with this technique. Steel bonding technique is simple, cost-effective and efficient. However, it was found that it suffers from a serious problem of deterioration of bond at the steel and concrete interphase due to corrosion of steel. Other common strengthening technique involves construction of steel jackets which is quite effective from strength, stiffness and ductility considerations. However, it increases overall cross-sectional dimensions, leading to increase in self-weight of structures and is labour intensive. To eliminate these problems, steel plate was replaced by corrosion resistant and light-weight FRPC plates. FRPCs help to increase strength and ductility without excessive increase in stiffness. Further, such material could be tailored to meet specific requirements by adjusting placement of fibers.

# 2.1.1. Flexural behavior of RC beams strengthened by FRPC

Flexural strengthening of RC beams using composites can be provided by epoxy bonding of FRPC plate to the portion of elements in tension, with fibers parallel to the principal stress direction. If fibers are placed perpendicular to cracks, a large increase in strength and stiffness is achieved compared to situation where fibers are placed oblique to the cracks [24,25]. Considerable experimental research has been conducted for strengthening of RC beams with glass, carbon or aramid FRPCs to investigate serviceability, strength enhancement, cracking patterns and failure-modes, etc. [26-52]. Literature review has shown that nearly 40% strength enhancement is possible for RC beams strengthened with glass fiber reinforced polymer composite (GFRPC) whereas around 200% strength enhancement is achieved with carbon fiber polymer composites (CFRPC). In addition to the fiber type, flexural performance of strengthened RC beams is affected by several factors such as modulus of elasticity of FRPC and its center of gravity location relative to the neutral axis [53], width of laminate [38], length of laminate [53], amount of main and shear reinforcement [54], number of FRPC layers [40], level of loading [55], FRPC configuration [56,57], concrete strength and cover [58], damage and loading condition [43,59], etc.

FRPC material has relatively low modulus of elasticity and linear stress-strain relation up to rupture with no definite yield point. As a result strengthened beams generally exhibit large deflection, wide as well as closer cracks and brittle failure mode [60,61]. Effect of reinforcement ratio on cracking moment, crack spacing, cracking patterns and crack width was experimentally investigated by Masmoudi et al. [62]. A variety of indices including deformability ratios [56], energy ratios [63] have been proposed to measure ductility because definition of ductility for steel reinforced concrete beam can not be directly applied to the FRPC strengthened RC beams. Experiments have indicated catastrophic failure of strengthened beams due to low ductility. Spadea et al. [36] and Bencardino et al. [64] have suggested anchorage system to increase ductility, which is not affected by the change in the loading rate [42]. Grace et al. [65,66] performed experiments by using innovative triaxially braided ductile fabric which was reported to increase ductility. It was reported by Salom et al. [67] that torsional capacity of RC beams can be increased up to 70% with the help of FRPC strengthening. Ghobarah et al. [68] demonstrated experimentally that fully wrapped beams performed better than only strips and 45° orientation of fibers is more effective for upgrading torsional resistance. To avoid the extensive time consuming process by employing semi-skilled labour for application of FRPC to concrete surface, a commercial off-the-shelf-actuated fastening system was used by Lamanna et al. [69] in experimental study by considering different fasters' length and layouts. The technique was reported to be effective for bonding compared to conventional techniques. This method also increased ductility over the conventionally

bonded method and took around 1/8 of time compared to the conventional method.

The quasi-static behavior of flexural members strengthened with FRPC is well documented in literature. However, there is a gap in knowledge on the effect of impact and fatigue loadings on the beam. Repeated loading can lead to internal cracks in a member which can alter its stiffness and load carrying characteristics. Barnes and Mays [70], Erki and Meier [71], Shahawy and Beitelman [72], Masoud et al. [73], Heffernan and Erki [74], Brena et al. [75] and Bonfiglioli et al. [76] presented experimental results for static and fatigue failure of beams strengthened with CFRPC sheets. It is observed from the results that fatigue life of reinforced concrete beams could be significantly enhanced through the use of externally bonded CFRPC laminate and it is largely dependent on the stress range applied to steel reinforcement.

The experimental studies discussed above have been substantiated by analytical approach at macro level. In all the simplified analytical models, strain compatibility has been used to predict flexural behavior either by ultimate load method or working stress method [9,29,46,77– 79], wherein issues related to rational design of externally strengthened RC beams for interpreting major modes of failure including flexural, interface separation, flexuralshear crack and concrete cover rip off have been addressed. Parametric study was performed by Picard et al. [80], which highlights the importance of concrete compressive strength whereas An et al. [81] emphasized on amount of the main reinforcement.

Stiffness of concrete structures usually starts to degrade, as cracks are developed in concrete. Stiffness degradation due to cracking of concrete is not considered in the simplified linear elastic models. Furthermore, contrary to actual behavior, stress-strain curve of concrete is assumed to be linear in elastic models. Therefore, it is necessary to account for the crack generation and stiffness degradation in refined non-linear analysis. Studies in this direction were performed using finite element method to capture flexural behavior of strengthened RC beams [82-86] by assuming perfect bonding between concretesteel and concrete-FRPC laminate. Thomsen et al. [87], for example, developed non-linear finite element models using bond-slip relationship between concrete and FRPC to evaluate delamination failure mode. On the other hand, Colotti et al. [88] proposed a theoretical model based on truss-analogy. A non-linear analysis was performed by Aiello and Ombres [89] considering tension stiffening and force transfer between concrete and FRPC to investigate serviceability (cracking and deformability) criteria. Yang et al. [90] presented fracture mechanics based finite element analysis to capture debonding failure. The method was observed to successfully simulate concrete cover separation failure mode in FRPC strengthened RC beams. Sato and Vecchio [91] developed a simple equation to estimate crack spacing, its width and tension stiffening effect.

#### 2.1.2. Shear behavior of RC beams strengthened by FRPC

Shear strengthening of RC elements can be provided by epoxy bonding of FRPC materials with fibers parallel, as practically possible, to the direction of the shear stresses. Various experimental and analytical works related to shear strengthening of beams with different FRPC laminates for uncracked/cracked RC beams are reported by Sharif et al. [92], Chajes et al. [93], Chaallal et al. [94], Triantafillou [95], Deniaud and Cheng [96], Lees et al. [97], Pellegrino and Modena [98], Adhikary and Mutsuyoshi [99], Zhang and Hsu [100]. It was observed that the shear strength of virgin beam can be increased by 60-120% using FRPC sheets. Fiber orientation may be vertical or perpendicular to the shear cracks. Shear contribution to the total shear capacity of strengthened RC beams depends on several parameter including surface preparation, composite fabric shear reinforcement ratio, amount of main and shear reinforcement, shear span to effective depth ratio, strength of FRPC, number of FRPC layers, wrapping schemes, depth of sheet across beam section [99,101–103]. U-wrap of sheet provided the most effective strengthening for RC beams with about 119% increase in shear strength.

The ultimate resistance of beam can not be taken into account by simple superposition of shear capacity contributions because of complex interaction between concrete, steel and FRPC. This has been reported to be the major obstacle in development of an analytical formula that can correctly predict the ultimate load of strengthened beams in shear [101,102]. By assuming a perfect bond between concrete and FRPC, Malek and Saadatmanesh [104,105] developed equilibrium and compatibility equations using truss analogy method. Further, compression field theory was used to calculate shear force resisted by FRPC plate, crack inclination angle, stresses in stirrups before cracking as well as after formation of crack. Khalifa et al. [106] reviewed research on shear strengthening and proposed a design algorithm to compute contribution of FRPC to shear capacity of RC beams. Another group of researchers [107–109] have presented analytical models to calculate the ultimate shear capacity of strengthened beams by assuming linear elastic behavior of FRPC materials. Review on different shear design methods can be found in Micelli et al. [110] with commentary on adequacy of each method. However, numerical modeling of shear strengthened RC beams with FRPC has not yet been addressed adequately in open literature.

#### 2.1.3. Durability of RC beams strengthened by FRPC

Seasonal and daily temperature variations cause freezing and thawing cycles, differential thermal expansion between concrete and FRPC substrate, resulting in premature plate separation and ultimately failure of strengthened system. Cross-directional (matrix dominated) properties such as transverse tensile/compressive strength and in-plane shear were found to be highly affected by environmental effects but fiber was less sensitive to it.

Karbhari and Engineer [111], Karbhari and Zhao [112], Sen et al. [113], Sen et al. [114,115], Green et al. [116], Aiello et al. [117]. Bisby and Green [118], examined effect of short-term environmental exposures on externally strengthened RC beams with FRPC by considering different types of fibers, different wet/dry and freeze/thaw cycles, etc. It was observed that degradation occurs primarily at the level of resin in contact with concrete and reduction in strength is nearly 80-90% when strengthened system is subjected to high temperature range [119]. A simple analytical model is proposed by Bisby and Green [118] to predict bond failure because of thermal load. Long-term behavior of strengthened beams is very important and work in this direction was reported by Karbhari and Engineer [111], Plevris and Triantafillou [120], Xie et al. [121], Karbhari and Shulley [122], Saadatmanesh and Tannous [123], Soudki and Sherwood [124] under various conditions like dry/ wet temperature, acids, alkali, etc. Creep and Shrinkage of strengthened beam was studied by Plevris and Triantafillou [120] and Bank et al. [125] who presented different test methods to study long-term behavior of FRPC structures along with different theoretical models and experimental techniques to predict effects of different environmental conditions. The combined effect of harsh environment and fatigue loading was studied by Gheorghiu et al. [126] on flexural behavior. Recently, Grace and Singh [127] proposed strength reduction factors associated with various independent environmental conditions like 100% humidity, salt water, alkali solution, freez-thaw, thermal expansion, etc. Effect of chloride content and rebar corrosion was studied by Wang et al. [128] whereas Maaddawy et al. [129] developed mathematical model for prediction of inelastic response of strengthened RC beams by taking into account reduction of steel area due to corrosion and its effect on concrete-steel interface.

### 2.1.4. Bond and development length of FRPC

Bond of external FRPC reinforcement to the concrete substrate is a critical factor for effectiveness of strengthening as delamination of FRPC laminate from concrete surface can cause failure of concrete structure. Arduini and Nanni [33], Arduini et al. [130], Buyukozturk and Hearing [131], Swamy and Mukhopadhyaya [132], Nakaba et al. [133], Nguyen et al. [134], Sebastian [135] and Lorenzis et al. [136] performed experimental studies to address bonding issue of FRPC plates. Experiments with different epoxies were also conducted by Saadatmanesh and Ehsani [26] who suggested use of rubber toughened epoxies. Bond between FRPC and concrete surface also depends on preparation of concrete surface (water jet or sand blasting), concrete compressive strength and effective bond length [137], fibers stiffness and shape of stress distribution [134], etc. Considerable research was performed by using anchor bolts or U-shape fiber fabrics at the end [32,132,138,139] to avoid premature failure of FRPC plates from concrete surface. This technique increases ductility but original concrete gets disturbed because of anchor bolt. This can be avoided by using U-shape fabrics which provide ductility as well as increased shear strength.

# 2.2. Strengthening of RC columns using FRPC

Wrapping of FRPC sheets around concrete columns is a promising method for structural strengthening and repair. Application of fabric sheet is quite easy, requiring no specialized tools; thus technique is of practical interest. One of the deficiencies in concrete columns is the lack of lateral confinement and low energy absorption capacity. External confinement of concrete significantly enhances strength, ductility and energy absorption capacity of concrete specimens by constructing additional RC cage around existing columns or using grout-injected steel jackets [140,141].

# 2.2.1. Axial behavior of RC columns strengthened with FRPC

A number of studies including Demers et al. [142], Nanni et al. [143], Saadatmanesh et al. [144], Seible et al. [145], Hanna and Jones [146], Xiao and Wu [147], Bousias et al. [148], Matthys et al. [149], Carey and Harries [150], Harajli [151] have investigated the axial behavior of concrete with different FRPC jackets from strength and ductility point of view. FRPC wraps consisting of carbon, aramid and glass fibers, bonded with epoxy resins have been successfully applied for seismic rehabilitation of bridge piers in USA and Japan [152]. Various parameters affecting the performance of confined columns' systems including concrete strength, depth-to-width ratio [153-155], longitudinal reinforcement, stirrups, corrosion of steel, concrete damage [156], fiber type, wrap angle [157], thickness of wrap [158], slenderness ratio [159], deformability of the concrete, stiffness of the jacket in the lateral direction [160], concrete dilation ratio [161], geometric and loading imperfection [162], etc. have been investigated by researchers. Application of pretensioned FRPC sheet for strengthening of RC columns has been performed by Mortazavi et al. [163].

Shape of column section is a critical parameter affecting confined strength of column. The most effective confinement is obtained for circular columns rather than rectangular and square columns [164–166]. Square or rectangular sections engage high confining pressure at their corners but little pressure on their flat sides, therefore the cross-section is not effectively confined, resulting in a lower increase in strength [142]. In order to increase the effectiveness of confinement for rectangular and square columns, the column section can be modified into the elliptical section, that is, the corners have to be rounded to prevent premature failure but radius is limited because of internal longitudinal reinforcement [164]. Shear strength of RC columns strengthened with CFRPC was studied by Ye et al. [167] who concluded that shear strength of RC column can be effectively increased with external strengthening.

Structural behavior of concrete columns confined by FRPC was investigated by many researchers [168–176]

using analytical models to predict stress-strain behavior between confined concrete and FRPC wraps. Analytical models are based on deformation compatibility and equilibrium of forces between concrete and FRPC. Mander et al. [140], for example, developed an analytical model to calculate increased compressive strength of concrete in RC column due to confining pressure provided by transverse reinforcement. This model was further modified by Teng and Lam [166], Wang and Restrepo [170], Tan [171], Saadatmanesh et al. [177] to analyze behavior of RC columns wrapped with FRPC of various cross-sections like circular, elliptical, square and rectangular. Mirmiran and Shahawy [178] modified model suggested by Mander et al. [140] by considering strain energy approach. A design procedure was proposed by Theriault and Neale [179] to improve axial load capacity of circular and rectangular columns confined with FRPC wraps. Chaallal et al. [180] presented a stress-strain curve by considering fibers in axial and lateral direction for axially loaded rectangular short columns confined with FRPC jackets. Lam and Teng [181] developed a stress-strain curve with fibers in hoop direction only, which can be directly used in design. This model is applicable for concrete confined by all types of FRPC as well as steel. Recently, comparisons of various available confinement models have been presented by Bisby et al. [182].

# 2.2.2. Seismic behavior of RC columns strengthened by FRPC

A large lateral cyclic earthquake force can degrade strength of concrete and reinforcing bar that can result in premature failure of column. Retrofitting of column components to withstand earthquakes is a recent and widespread task and one of the more complex engineering challenges. Seismic resistance of retrofitted RC columns improves significantly because of confining action of the FRPC wraps [183–185]. The technique has been observed to improve displacement ductility as well as strength. Further, repaired specimens exhibit lower rate of deterioration under large reversal cyclic loading than the virgin columns [186]. Amount of external reinforcement required depends on level of axial load and extent of damage.

Xiao and Ma [187] developed an analytical model by considering the bond-slip deterioration of lap spliced longitudinal bars for seismic assessment and retrofit design. A non-linear finite element analysis was performed by Parvin and Wang [188] on FRPC jacketed RC column under combined axial and cyclic lateral loading. Finite element analysis results indicated that FRPC fabric showed significant improvement in strength as well as ductility in potential plastic hinge location at the bottom of column. Elsanadedy and Haroun [189] proposed seismic design procedure for circular lap-splice reinforced RC column upgraded with FRPC jackets based on moment curvature analysis with inclusion of bond-slip mechanism.

#### 2.2.3. Durability of RC columns strengthened by FRPC

Environmental exposures to conditions such as freezethaw can potentially affect confining material (FRPC) as well as confined concrete and the bond between composite and concrete. Exposure of various environmental conditions usually resulted in decrease of strength, stiffness, and possibility of change in failure mode [190-195]. Toutanji and Balaguru [196,197] reported that CFRPC is superior to GFRPC under harsh environment. It was observed that exposure to wet-dry environments has little effect on strength and ductility of CFRPC wrapped specimens. On the other hand, GFRPC wrapped specimens exhibited about 10% reductions in strength. However, CFRPC and GFRPC wrapped specimens are equally susceptible to freeze-thaw cycles. Another group of researchers [198-200] performed experimental studies on strengthening of corrosion damaged RC columns by using different types of fibers and concluded nearly 20% increase in load carrying capacity with 50% decrease in rate of post repair corrosion but the strengthened system exhibited somewhat reduced ductility because of loss of reinforcement due to corrosion process.

# 2.3. Strengthening of RC beam-columns joint by FRPC

Performance of beam-column joints is very important in determination of the ability of structure to withstand large earthquake and other lateral loads. Shear failure of beamcolumn joints has been identified to be the principal cause for collapse of many moment resisting frame buildings during recent earthquakes. Shear failure during an earthquake have been attributed to inadequate transverse reinforcements at the joint and weak-columns/strong-beam design. A study on external beam-column joint has shown failure of the structure by beam hinging [201] if axial load on the columns is high and beam reinforcement is less than 1.2%. Several techniques have been applied to strengthen beam-column joints, including uses of concrete jackets, bolted steel plates [202]. However, it is difficult to provide effective confinement in the rehabilitation of beam-column joints. Use of FRPC for strengthening of dilapidated reinforced concrete structures has increased in recent years. However, behavior of beam-column connection is complex and still not completely understood. External FRPC reinforcement is an effective method to increase moment carrying capacity of beam-column connection by about 60% [203] and shear capacity of the joint by about 35% [204,205].

Various researchers have conducted experiments on strengthening of beam-column joints from a ductility point of view to understand failure mode with and without anchorage using different types of FRPC with variable angle of fibers and numbers of layers [205–210]. It has been observed that fibers inclined at 45° to the direction of principal planes are most effective for strengthening in the joint region. Pulido et al. [211], Shannag and Alhassan [212] performed experimental studies on seismic behavior of beam-column joints. Pulido et al. [211] also proposed a simple model and implemented confined concrete stress–strain curve in pushover analysis.

#### 3. General concluding remarks

Application of FRPCs in civil construction both in repair and retrofitting has been reviewed. Both experimental and analytical works have been included. Application of FRPCs for slab are not discussed here for the sake of brevity; only few pertinent literature is listed at the end [213–229]. Following general concluding remarks are made:

- Majority of research has been concentrated on repair of existing structures. Studies have demonstrated improvement in ultimate capacity and stiffness leading to reduction in the overall maximum deflection and strains. To utilize the full capacity of the FRPC plate and to prevent the plate separation, plate anchorage system can be advantageously used to improve bond strength between FRPC and concrete as it is the key factor affecting the overall integrity of beams.
- Confinement to concrete columns provided in the form of wrapping of FRPC fabrics or tubes has proved extremely beneficial. This has achieved enhancement in strength, load carrying capacity, energy absorption, ductility, stiffness and improvement in failure-modes and hence, proved extremely beneficial for concrete columns. Extent of benefit, however, depends upon many factors such as type, amount, and direction of confining material, size, shape and loading condition of the column.
- Externally bonded FRPC reinforcement is a viable solution towards enhancing strength, stiffness and energy dissipation characteristics of reinforced concrete beamcolumn joints subjected to regular as well as seismic loads. It also enhances shear capacity and improves overall damage control.
- Use of FRPC improves load carrying capacity and energy absorption capability of slabs reinforced with FRPC. General cohesiveness, stress transfer capability across the crack improves due to strengthening, which delays crack formation and thus FRPC reinforcement is able to achieve its full potential of strengthening of slabs.
- Research is needed to determine the endurance limit of FRPC during fire, fatigue performance of strengthened structure, effect of chemical and ultra-violet radiation on FRPC, etc. Long term studies are required to examine effect of alkalinity, temperature, etc. on resins and fibers. Effect of freeze-thaw cycling under sustained load is also not understood fully. Width of laminate is not entirely effective in resisting moments in the end zone; behavior of beams with varying widths of laminate towards the end can also be investigated. Research is needed to study behavior of short as well as long columns under combined axial and bending moment.

Column subjected to dynamic loading condition is another important area for consideration. Experimental and analytical studies are required to understand behavior of beam-column joints from torsion, ductility and durability points of view.

# Acknowledgements

Partial support of USIF Indo-US Collaborative Sponsored Research Project IND104 (95IU001) is gratefully acknowledged. Constructive comments of the reviewer are also gratefully acknowledged.

# References

- [1] ACI Committee-503. Guide for the selection of polymer adhesive with concrete. ACI Mater J 1992;89(1):90–105.
- [2] Uomoto T, Mutsuyoshi H, Katsuki F, Misra S. Use of fiber reinforced polymer composites as reinforcing material for concrete. ASCE J Mat Civil Eng 2002;14(3):191–209.
- [3] Karbhari VM. Materials consideration in FRP rehabilitation of concrete structures. ASCE J Mat Civil Eng 2001;13(2):90–7.
- [4] Einde LVD, Zhao L, Seible F. Use of FRP composites in civil structural application. Constr Build Mater 2003;17:389–403.
- [5] Bank LC, Gentry TR, Thompson BP, Russell JS. A model specification of FRP composites for civil engineering structures. Constr Build Mater 2003;17:405–37.
- [6] Bakht B, Al-Bazi G, Banthia N, Cheung M, Erki MA, Faoro M, et al. Canadian bridge design code provisions for fiber-reinforced structures. ASCE J Compos Const 2000;4(1):3–15.
- [7] ACI Committee 440. Guide for the design and construction of externally bonded FRP system for strengthening concrete structures. Farmington Hill, MI: American Concrete Institute; 2002.
- [8] Nanni A. North American design guidelines for concrete reinforcement and strengthening using FRP: Principles, applications and unresolved issues. Constr Build Mater 2003;17:439–46.
- [9] Nanni A. Flexural behavior and design of RC members using FRP reinforcement. ASCE J Struct Eng 1993;119(11):3344–58.
- [10] Mufti AA, Labossiere P, Neale KW. Recent bridge application of FRPCs in Canada. Struct Eng Int 2002;2:96–8.
- [11] Hollaway LC. The evolution of and the way forward for advanced polymer composites in the civil infrastructure. Constr Build Mater 2003;17:365–78.
- [12] Mufti AA. FRPs and FOSs lead to innovation in Canadian civil engineering structures. Constr Build Mater 2003;17:379–87.
- [13] Meier U. Carbon fiber reinforced polymers: modern materials in bridge engineering. Struct Eng Int 1992;1:7–12.
- [14] Saadatmanesh H. Fiber composites for new and existing structures. ACI Struct J 1994;91(3):346–54.
- [15] ACI Committee 440. State-of-the-Art report on fiber reinforced plastic (FRP) reinforcement for concrete structures. Farmington Hill, MI: American Concrete Institute; 1996.
- [16] Bakis CE, Bank LC, Brown VL, Cosenza E, Davalos JF, Lesko JJ, et al. Fiber-reinforced polymer composites for construction – stateof-the-art review. ASCE J Compos Const 2002;6(2):73–87.
- [17] Deniaud C, Cheng JJR. Review of shear design methods for reinforced concrete beams strengthened with fibre reinforced polymer sheets. Can J Civil Eng 2001;28:271–81.
- [18] Bousselham A, Chaallal O. Shear strengthening reinforced concrete beams with fiber-reinforced polymer: Assessment of influencing parameters and required research. ACI Struct J 2004;101(2): 219–27.
- [19] Lu XZ, Teng JG, Ye LP, Jiang JJ. Bond-slip models for FRP sheet/ plates bonded to concrete. Eng Struct 2005;27:920–37.

- [20] Engindeniz M, Kahn LF, Zureick AH. Repair and strengthening of reinforced concrete beam-column joints – State of the art. ACI Struct J 2005;102(2):187–97.
- [21] Fardis MN, Khalili H. FRP encased concrete as a structural material. Mag Concrete Res 1982;34(121):191–202.
- [22] Swamy RN, Jones R, Bloxham JW. Structural behaviour of reinforced concrete beams strengthened by epoxy-bonded steel plates. The Struct Eng A 1987;65(2):59–68.
- [23] Hamoush SA, Ahmad SH. Static strength tests of steel plate strengthened concrete beams. Mater Struct 1990;23:116–25.
- [24] Norris T, Saadatmanesh H, Ehsani MR. Shear and flexural strengthening of R/C beams with carbon fiber sheets. ASCE J Struct Eng 1997;23(7):903–11.
- [25] Grace NF, Sayed GA, Soliman AK, Saleh KR. Strengthening reinforced concrete beams using fiber reinforced polymer (FRP) laminate. ACI Struct J 1999;96(5):865–74.
- [26] Saadatmanesh H, Ehsani MR. Flexural strength of externally reinforced concrete beams, Serviceability and durability of construction material. Proc First ASCE Mater Eng Congress 1990;Part-2:1152–61.
- [27] Saadatmanesh H, Ehsani MR. Fiber composite plates can strengthen beams. ACI Con Int Design Const 1990;12(3):65–71.
- [28] Ritchie PA, Thomas DA, Lu LW, Connelly GM. External reinforcement of concrete beams using fiber reinforced plastics. ACI Struct J 1991;88(4):490–500.
- [29] Triantafillou TC, Plevris N. Strengthening of RC beams with epoxybonded fibre composite materials. Mater Struct 1992;25:201–11.
- [30] Faza SS, GangaRao HVS. Fiber composite wrap for rehabilitation of concrete structures. Proc Mater Eng Conf, ASCE 1994;804:1135–9.
- [31] Benmokrane B, Chaallal O, Masmoudi R. Flexural response of concrete beams reinforced with FRP reinforcing bars. ACI Mater J 1996;91(2):46–55.
- [32] Garden HN, Hollaway LC. An experimental study of the influence of plate end anchorage of carbon fibre composite plates used to strengthen reinforced concrete beams. Compos Struct 1998;42:175–88.
- [33] Arduini M, Nanni A. Behavior of precracked RC beams strengthened with carbon FRP sheets. ASCE J Compos Const 1997;1(2):63–70.
- [34] Arduini M, Nanni A. Parametric study of beams with externally bonded FRP reinforcement. ACI Struct J 1997;94(5):493–501.
- [35] Mukhopadhyaya P, Swamy N, Lynsdale C. Optimizing structural response of beams strengthened with GFRP plates. ASCE J Compos Const 1998;2(2):87–95.
- [36] Spadea G, Bencardino F, Swamy RN. Structural behavior of composite RC beams with externally bonded CFRP. ASCE J Compos Const 1998;2(3):132–7.
- [37] Santhakumar R, Kannabiran S, Dhanaraj R. Strengthening of reinforced concrete beams using glass fibre reinforced plastic laminates. The Indian Con J 1999:737–40.
- [38] Ramana VPV, Kant T, Morton SE, Dutta PK, Mukherjee A, Desai YM. Behavior of CFRPC strengthened reinforced concrete beams with varying degrees of strengthening. Compos: Part B 2000;31:461–70.
- [39] Labossiere P, Neale KW, Rochette P, Demers M, Lamothe P, Lapierre P, et al. Fibre reinforced polymer strengthening of the Sainte-Emelie-de-l'Energie bridge: design, instrumentation, and field testing. Can J Civil Eng 2000;27:916–27.
- [40] Shahawy M, Chaallal O, Beitelman TE, El-Saad A. Flexural strengthening with carbon fiber-reinforced polymer composites of preloaded full-scale girders. ACI Struct J 2001;98(5):735–42.
- [41] Grace NF. Strengthening of negative moment region of reinforced concrete beams using carbon fiber-reinforced polymer strips. ACI Struct J 2001;98(3):347–58.
- [42] White TW, Soudki KA, Erki MA. Response of RC beams strengthened with CFRP laminates and subjected to a high rate of loading. ASCE J Compos Const 2001;5(3):153–62.

- [43] Bonacci JF, Maalej M. Behavioral trends of RC beams strengthened with externally bonded FRP. ASCE J Compos Const 2001;5(2):102–13.
- [44] Hag-Elsafi O, Alampalli S, Kunin J. Application of FRP laminates for strengthening of a reinforced-concrete T-beam bridge structure. Compos Struct 2001;52:453–66.
- [45] Sheikh SA, DeRose D, Mardukhi J. Retrofitting of concrete structures for shear and flexure with fiber-reinforced polymers. ACI Struct J 2002;99(4):451–9.
- [46] Malek AM, Patel K. Flexural strengthening of reinforced concrete flanged beams with composite laminates. ASCE J Compos Const 2002;6(2):97–103.
- [47] Taheri F, Shahin K, Widiarsa I. On the parameters influencing the performance of reinforced concrete beams strengthened with FRP plates. Compos Struct 2002;58:217–26.
- [48] Sheikh S. Performance of concrete structures retrofitted with fibre reinforced polymers. Eng Struct 2002;4:869–79.
- [49] Brena SF, Bramblett RM, Wood SL, Kreger ME. Increasing flexural capacity of reinforced concrete beams using carbon fiber-reinforced polymer composites. ACI Struct J 2003;100(1):36–46.
- [50] Limam O, Foret G, Ehrlacher A. RC beams strengthened with composite material: a limit analysis approach and experimental study. Compos Struct 2003;59:467–72.
- [51] Tavakkolizadeh M, Saadatmanesh H. Strengthening of steel-concrete composite girders using carbon fiber reinforced polymer sheets. ASCE J Struct Eng 2003;129(1):30–40.
- [52] Vougioukas E, Zeris CA, Kotsovos MD. Towards safe and efficient use of fiber-reinforced polymer for repair and strengthening of reinforced concrete structures. ACI Struct J 2005;102(4):525–34.
- [53] Heffernan PJ, Erki MA. Equivalent capacity and efficiency of reinforced concrete beams strengthened with carbon fibre reinforced plastic sheets. Can J Civil Eng 1996;23:21–9.
- [54] Rahimi H, Hutchinson A. Concrete beams strengthened with externally bonded FRP plates. ASCE J Compos Const 2001;5(1):44–56.
- [55] Shin YS, Lee C. Flexural behavior of reinforced concrete beams strengthened with carbon fiber-reinforced polymer laminates at different levels of sustaining load. ACI Struct J 2003;100(2): 231–9.
- [56] GangaRao HVS, Vijay PV. Bending behavior of concrete beams wrapped with carbon fabric. ASCE J Struct Eng 1998;124(1):3–10.
- [57] Brena SF, Macri BM. Effect of carbon-fiber-reinforced polymer laminate configuration on the behavior of strengthened reinforced concrete beams. ASCE J Compos Const 2004;8(3):229–40.
- [58] Wu ZS, Yoshizawa H. Analytical/experimental study on composite behavior in strengthening structures with bonded carbon fiber sheets. J Reinf Plast Compos 1999;18(12):1131–55.
- [59] Bonacci JF, Maalej M. Externally bonded fiber-reinforced polymer for rehabilitation of corrosion damage concrete beams. ACI Struct J 2000;97(5):703–11.
- [60] Pecce M, Manfredi G, Cosenza E. Experimental response and code models of GFRP RC beams in bending. ASCE J Compos Const 2000;4(4):182–90.
- [61] Razaqpur AG, Svecova D, Cheung MS. Rational method for calculating deflection of fiber-reinforced polymer beams. ACI Struct J 2000;97(1):175–84.
- [62] Masmoudi R, Benmokrane B, Chaallal O. Cracking behaviour of concrete beams reinforced with fiber reinforced plastic rebars. Can J Civil Eng 1996;23:1172–9.
- [63] Grace NF, Soliman AK, Abdel-Sayed G, Saleh KR. Behavior and ductility of simple and continuous FRP reinforced beams. ASCE J Compos Const 1998;2(4):186–94.
- [64] Bencardino F, Spadea G, Swamy RN. Strength and ductility of reinforced concrete beams externally reinforced with carbon fiber fabric. ACI Struct J 2002;99(2):163–71.
- [65] Grace NF, Abdel-Sayed G, Ragheb WF. Strengthening of concrete beams using innovative ductile fiber-reinforced polymer fabric. ACI Struct J 2002;99(5):692–700.

- [66] Grace NF, Ragheb WF, Abdel-Sayed G. Strengthening of cantilever and continuous beams using new triaxially braided ductile fabric. ACI Struct J 2004;101(2):237–44.
- [67] Salom PR, Gergely J, Young DT. Torsional strengthening of spandrel beams with fiber-reinforced polymer laminates. ASCE J Compos Const 2004;8(2):157–62.
- [68] Ghobarah A, Ghorbel MN, Chidiac SE. Upgrading torsional resistance of reinforced concrete beams using fiber-reinforced polymer. ASCE J Compos Const 2002;6(4):257–63.
- [69] Lamanna AJ, Bank LC, Scott DW. Flexural strengthening of reinforced concrete beams by mechanically attaching fiberreinforced polymer strips. ASCE J Compos Const 2004;8(3): 203–10.
- [70] Barnes RA, Mays GC. Fatigue performance of concrete beams strengthened with CFRP plates. ASCE J Compos Const 1999;3(2):63–72.
- [71] Erki MA, Meier U. Impact loading of concrete beams externally strengthened with CFRP laminates. ASCE J Compos Const 1999;3(3):117–24.
- [72] Shahawy M, Beitelman TE. Static and fatigue performance of RC beams strengthened with CFRP laminates. ASCE J Struct Eng 1999;125(6):613–21.
- [73] Masoud S, Soudki K, Topper T. CFRP-strengthened and corroded RC beams under monotonic and fatigue loads. ASCE J Compos Const 2001;5(4):228–36.
- [74] Heffernan PJ, Erki MA. Fatigue behavior of reinforced concrete beams strengthened with carbon fiber reinforced plastic laminates. ASCE J Compos Const 2004;8(2):132–40.
- [75] Brena SF, Benouaich MA, Kreger ME, Wood SL. Fatigue tests of reinforced concrete beams strengthened using carbon fiber-reinforced polymer composites. ACI Struct J 2005;102(2):305–13.
- [76] Bonfiglioli B, Pascale G, Mingo SM. Dynamic testing of reinforced concrete beams damaged and repaired with fiber reinforced polymer sheets. ASCE J Mater Civil Eng 2004;16(5):400–6.
- [77] Ziraba YN, Baluch MH, Basunbul IA, Sharif AM, Azad AK, Al-Sulaimani GJ. Guidelines towards the design of reinforced concrete beams with external plates. ACI Struct J 1994;91(6):639–46.
- [78] Vijay PV, GangaRao HVS. Bending behavior and deformability of glass fiber-reinforced polymer reinforced concrete members. ACI Struct J 2001;98(6):834–42.
- [79] Teng JG, Smith ST, Yao J, Chen JF. Intermediate crack-induced debonding in RC beams and slabs. Constr Build Mater 2003;17:447–62.
- [80] Picard A, Massicotte B, Boucher E. Strengthening of reinforced concrete beams with composite materials: theoretical study. Compos Struct 1995;33:63–75.
- [81] An W, Saadatmanesh H, Ehsani MR. RC beams strengthened with FRP plates II: analysis and parametric study. ASCE J Struct Eng 1991;117(11):3434–55.
- [82] Ross CA, Jerome DM, Tedesco JW, Hughes ML. Strengthening of reinforced concrete beams with externally bonded composite laminates. ACI Struct J 1999;96(2):212–20.
- [83] Tedesco JW, Stallings JM, El-Mihilmy M. Finite element method analysis of a concrete bridge repaired with fiber reinforced plastic laminates. Comput Struct 1999;72:379–407.
- [84] Sen R, Carpenter W, Snyder D. Finite element modeling of fiber reinforced polymer pretensioned elements subjected to environmental loads. ACI Struct J 1999;96(5):766–73.
- [85] Kachlakev D, Miller T, Yim S, Chansawat K, Potisuk T. Strengthening bridges using composite materials. FHWA-OR-RD-98-08, Oregon Department of Transportation, Salem, OR; 1998.
- [86] Buyle-Bodin F, David E, Ragneau E. Finite element modeling of flexural behaviour of externally bonded CFRP reinforced concrete structures. Eng Struct 2002;24:1423–9.
- [87] Thomsen H, Spacone E, Limkatanyu S, Camata G. Failure mode analyses of reinforced concrete beams strengthened in flexure with externally bonded fiber-reinforced polymers. ASCE J Compos Const 2004;8(2):123–31.

- [88] Colotti V, Spadea G, Swamy RN. Structural model to predict the failure behavior of plated reinforced concrete beams. ASCE J Compos Const 2004;8(2):104–22.
- [89] Aiello MA, Ombres L. Cracking and deformability analysis of reinforced concrete beams strengthened with externally bonded carbon fiber reinforced polymer sheets. ASCE J Mater Civil Eng 2004;16(5):392–9.
- [90] Yang ZJ, Chen JF, Proverbs D. Finite element modeling of concrete cover separation failure in FRP plated RC beams. Constr Build Mater 2003;17:3–13.
- [91] Sato Y, Vecchio FJ. Tension stiffening and crack formation in reinforced concrete members with fiber-reinforced polymer sheets. ASCE J Struct Eng 2003;129(6):717–24.
- [92] Sharif A, Al-Sulamani GJ, Basunbul IA, Baluch MH, Ghaleb BN. Strengthening of initially loaded reinforced concrete beams using FRP plates. ACI Struct J 1994;91(2):160–8.
- [93] Chajes MJ, Januszka TF, Mertz DR, Thomson TA, Finch WW. Shear strengthening of reinforced concrete beams using externally applied composite fabrics. ACI Struct J 1995;92(3):295–303.
- [94] Chaallal O, Nollet MJ, Perraton D. Shear strengthening of RC beams by externally bonded side CFRP strips. ASCE J Compos Const 1998;2(2):111–4.
- [95] Triantafillou TC. Shear strengthening of reinforced concrete beams using epoxy-bonded FRP composites. ACI Struct J 1998;95(2):107–15.
- [96] Deniaud C, Cheng JJR. Shear behavior of reinforced concrete Tbeams with externally bonded fiber-reinforced polymer sheets. ACI Struct J 2001;98(3):386–94.
- [97] Lees JM, Winistorfer AU, Meier U. External prestressed carbon fiber-reinforced polymer straps for shear enhancement of concrete. ASCE J Compos Const 2002;6(4):249–55.
- [98] Pellegrino C, Modena C. Fiber reinforced polymer shear strengthening of reinforced concrete beams with transverse steel reinforcement. ASCE J Compos Const 2002;6(2):104–11.
- [99] Adhikary BB, Mutsuyoshi H. Behavior of concrete beams strengthened in shear with carbon-fiber sheets. ASCE J Compos Const 2004;8(3):258–64.
- [100] Zhang Z, Hsu CTT. Shear strengthening of reinforced concrete beams using carbon-fiber-reinforced polymer laminates. ASCE J Compos Const 2005;9(2):158–69.
- [101] Li A, Assih J, Delmas Y. Shear strengthening of RC beams with externally bonded CFRP sheets. ASCE J Struct Eng 2001;127(4):374–80.
- [102] Li A, Diagana C, Delmas Y. CFRP contribution to shear capacity of strengthened RC beams. Eng Struct 2001;23:1212–20.
- [103] Chaallal O, Shahawy M, Hussan M. Performance of reinforced concrete T-girders strengthened in shear with carbon fiber-reinforced polymer fabric. ACI Struct J 2002;99(3):335–43.
- [104] Malek AM, Saadatmanesh H. Analytical study of reinforced concrete beams strengthened with web-bonded fiber reinforced plastic plates or fabrics. ACI Struct J 1998;95(3):343–52.
- [105] Malek AM, Saadatmanesh H. Ultimate shear capacity of reinforced concrete beams strengthened with web-bonded fiber-reinforced plastic plates. ACI Struct J 1998;95(4):391–9.
- [106] Khalifa A, Gold WJ, Naani A, Aziz A. Contribution of externally bonded FRP to shear capacity of RC flexural members. ASCE J Compos Const 1998;2(4):195–202.
- [107] Ibell T, Burgoyne C. Use of fiber-reinforced plastics versus steel for shear reinforcement of concrete. ACI Struct J 1999;96(6):997–1002.
- [108] Gendron G, Picard A, Guerin MC. A theoretical study on shear strengthening of reinforced concrete beams using composite plates. Compos Struct 1999;45:303–9.
- [109] Triantafillou TC, Antonopoulos CP. Design of concrete flexural members strengthened in shear with FRP. ASCE J Compos Const 2000;4(4):198–205.
- [110] Micelli F, Annaiah RH, Nanni A. Strengthening of short shear span reinforced concrete T joists with fiber-reinforced plastic composites. ASCE J Compos Const 2002;6(4):264–71.

- [111] Karbhari VM, Engineer M. Effect of environmental exposure on the external strengthening of concrete with composite – short term bond durability. J Reinf Plast Compos 1996;15:1194–216.
- [112] Karbhari VM, Zhao L. Issues related to composite plating and environmental exposure effects on composite–concrete interface in external strengthening. Compos Struct 1998;40(3-4):293–304.
- [113] Sen R, Shahawy M, Rosas J, Sukumar S. Durability of aramid pretensioned elements in a marine environment. ACI Struct J 1998;95(5):578–87.
- [114] Sen R, Shahawy M, Rosas J, Sukumar S. Durability of aramid fiber reinforced plastic pretensioned elements under tidal/thermal cycles. ACI Struct J 1999;96(1):95–106.
- [115] Sen R, Shahawy M, Sukumar S, Rosas J. Durability of carbon fiber reinforced polymer (CFRP) pretensioned elements under tidal/ thermal cycles. ACI Struct J 1999;96(3):450–7.
- [116] Green MF, Bisby LA, Beaudoin Y, Labossiere P. Effect of freezethaw cycles on the bond durability between fibre reinforced polymer plate reinforcement and concrete. Can J Civil Eng 2000;27:949–59.
- [117] Aiello MA, Focacci F, Nanni A. Effects of thermal loads on concrete cover of fiber-reinforced polymer reinforced elements: theoretical and experimental analysis. ACI Mater J 2001;98(4):332–9.
- [118] Bisby LA, Green MF. Resistance to freezing and thawing of fiberreinforced polymer-concrete bond. ACI Struct J 2002;99(2): 215–23.
- [119] Katz A, Berman N, Bank LC. Effect of high temperatures on bond strength of FRP rebars. ASCE J Compos Const 1999;3(2):73–81.
- [120] Plevris N, Triantafillou TC. Time-dependent behavior of RC members strengthened with FRP laminates. ASCE J Struct Eng 1994;120(3):1016–42.
- [121] Xie M, Hoa SV, Xiao XR. Bonding steel reinforced concrete with composites. J Reinf Plast Compos 1995;14:949–63.
- [122] Karbhari VM, Shulley SB. Use of composites for rehabilitation of steel structures – determination of bond durability. ASCE J Mater Civil Eng 1995;7(4):239–45.
- [123] Saadatmanesh H, Tannous FE. Long term behavior of aramid fiber reinforced plastic (AFRP) tendons. ACI Mater J 1999;96(3):297–305.
- [124] Soudki KA, Sherwood TG. Behaviour of reinforced concrete beams strengthened with carbon fibre reinforced polymer laminates subjected to corrosion damage. Can J Civil Eng 2000;27: 1005–10.
- [125] Bank LC, Gentry TR, Barkatt A. Accelerated test methods to determine the long-term behavior of FRP composite structures: environmental effects. J Reinf Plast Compos 1995;14:559–87.
- [126] Gheorghiu C, Labossiere P, Raiche A. Environmental fatigue and static behavior of RC beams strengthened with carbon-fiberreinforced polymer. ASCE J Compos Const 2004;8(3):211–8.
- [127] Grace NF, Singh SB. Durability evaluation of carbon fiberreinforced polymer strengthened concrete beams: experimental study and design. ACI Struct J 2005;102(1):40–53.
- [128] Wang CY, Shih CC, Hong SC, Hwang WC. Rehabilitation of cracked and corroded reinforced concrete beams with fiber-reinforced plastic patches. ASCE J Compos Const 2004;8(3):219–28.
- [129] Maaddawy TE, Soudki K, Topper T. Computer-based mathematical model for performance prediction of corroded beams repaired with fiber reinforced polymer. ASCE J Compos Const 2005;9(3):227–35.
- [130] Arduini M, Tommaso AD, Nanni A. Brittle failure in FRP plate and sheet bonded beams. ACI Struct J 1997;94(4):363–70.
- [131] Buyukozturk O, Hearing B. Failure behavior of precracked concrete beams retrofitted with FRP. ASCE J Compos Const 1998;2(3):138–44.
- [132] Swamy RN, Mukhopadhyaya P. Debonding of carbon-fibre-reinforced polymer plate from concrete beams. Proc Inst Civil Eng Struct Build 1999;134:301–17.
- [133] Nakaba K, Kanakubo T, Furuta T, Yoshizawa H. Bond behavior between fiber reinforced polymer laminates and concrete. ACI Struct J 2001;98(3):359–67.

- [134] Nguyen DM, Chan TK, Cheong HK. Brittle failure and bond development length of CFRP concrete beams. ASCE J Compos Const 2001;5(1):12–7.
- [135] Sebastian WM. Significance of midspan debonding failure in FRPplated concrete beams. ASCE J Struct Eng 2001;127(7):792–8.
- [136] Lorenzis LD, Miller B, Nanni A. Bond of fiber-reinforced polymer laminates to concrete. ACI Mater J 2001;98(3):256–64.
- [137] Chajes MJ, Finch WW, Januszka TF, Thomson TA. Bond and force transfer of composite materials plates bonded to concrete. ACI Struct J 1996;93(2):208–17.
- [138] Taljsten B. Defining anchor lengths of steel and CFRP plates bonded to concrete. Int J Adhes Adhes 1997;17(4):319–27.
- [139] Bizindavyi L, Neale KW. Transfer lengths and bond strength for composites bonded to concrete. ASCE J Compos Const 1999;3(4):153–60.
- [140] Mander JB, Priestley MJN, Park R. Theoretical stress-strain model for confined concrete. ASCE J Struct Eng 1998;114(8):1804–26.
- [141] Chai YH, Preiestley MJN, Seible F. Seismic retrofit of circular bridge columns for enhanced flexural performance. ACI Struct J 1991;88(5):572–84.
- [142] Demers M, Hebert D, Labossiere P, Neale KW. The strengthening of structural concrete with an aramid woven fibre/epoxy resin composite. Proceedigns of the advanced composite materials in bridges and structures. Montreal: Canadian Society for Civil Engineering; 1996. p. 435–42.
- [143] Nanni A, Norris MS, Bradford NM. Lateral confinement of concrete using FRP reinforcement. ACI SP-138: fibre reinforced plastic reinforcement for concrete structures. Detroit: American Concrete Institute; 1992. p. 193–209.
- [144] Saadatmanesh H, Ehsani MR, Jin L. Seismic strengthening of circular bridge pier models with fiber composites. ACI Struct J 1996;93(6):639–47.
- [145] Seible F, Priestley MJN, Hegemier GA, Innamorato D. Seismic retrofit of RC columns with continuous carbon fiber jackets. ASCE J Compos Const 1997;1(2):52–62.
- [146] Hanna S, Jones R. Composite wraps for aging infrastructure: concrete columns. Compos Struct 1997;38(1-4):57-64.
- [147] Xiao Y, Wu H. Compressive behavior of concrete confined by carbon fiber composite jackets. ASCE J Mater Civil Eng 2000;12(2):139–46.
- [148] Bousias SN, Triantafillou TC, Fardis MN, Spathis L, O'Regan BA. Fiber-reinforced polymer retrofitting of rectangular reinforced concrete columns with or without corrosion. ACI Struct J 2004;101(4):512–20.
- [149] Matthys S, Toutanji H, Audenaert K, Taerwe L. Axial load behavior of large-scale columns with fiber-reinforced polymer composites. ACI Struct J 2005;102(2):258–67.
- [150] Carey SA, Harries KA. Axial behavior and modeling of confined small-medium and large-scale circular section with carbon fiberreinforced polymer jackets. ACI Struct J 2005;102(4):596–604.
- [151] Harajli MH. Behavior of gravity load-designed rectangular concrete columns confined with fiber-reinforced polymer sheets. ASCE J Compos Const 2005;9(1):4–14.
- [152] Mufti AA, Erki MA, Jaeger LC. Advanced composite materials in bridge and structures in Japan. Montreal, Canada: Canadian Soc Civil Eng; 1992.
- [153] Ilki A, Kumbasar N, Koc V. Low strength concrete members externally confined with FRP sheets. Struct Eng Mech 2004;18(2):167–94.
- [154] Hamad BS, Rteil AA, Salwan BR, Soudki KA. Behavior of bondcritical regions wrapped with fiber-reinforced polymer sheets in normal and high-strength concrete. ASCE J Compos Const 2004;8(3):248–57.
- [155] Li B, Park R. Confining reinforcement for high-strength concrete columns. ACI Struct J 2004;101(3):314–24.
- [156] Demers M, Neale KW. Confinement of reinforced concrete columns with fibre-reinforced composite sheets- an experimental study. Can J Civil Eng 1999;26:226–41.

- [157] Mukherjee A, Ramana VPV, Kant T, Dutta PK, Desai YM. Discussion on behavior of concrete confined by fibre composites. ASCE J Struct Eng 1998;124(9):1094–5.
- [158] Ilki A, Kumbasar N. Behavior of damaged and undamaged concrete strengthened by carbon fiber composite sheets. Struct Eng Mech 2002;13(1):75–90.
- [159] Mirmiran A, Shahawy M, Beitleman T. Slenderness limit for hybrid FRP-concrete columns. ASCE J Compos Const 2001;5(1):26–34.
- [160] Chaallal O, Shahawy M. Performance of fiber-reinforced polymerwrapped reinforced concrete column under combined axial-flexural loading. ACI Struct J 2000;97(4):659–68.
- [161] Pessiki S, Harries KA, Kestner JT, Sause R, Ricles JM. Axial behavior of reinforced concrete columns confined with FRP jackets. ASCE J Compos Const 2001;5(4):237–45.
- [162] Mukherjee A, Boothby TE, Bakis CE, Joshi MV, Maitra SR. Mechanical behavior of fiber-reinforced polymer-wrapped concrete columns – complicating effects. ASCE J Compos Const 2004;8(2):97–103.
- [163] Mortazavi AA, Pilakoutas K, Son KS. RC column strengthening by lateral pre-tensioning of FRP. Constr Build Mater 2003;17:491–7.
- [164] Rochette P, Labossiere P. Axial testing of rectangular columns models confined with composites. ASCE J Compos Const 2000;4(3):129–36.
- [165] Mirmiran A, Shahawy M, Samaan M, Echary HE, Mastrapa JC, Pico O. Effect of column parameters on FRP confined concrete. ASCE J Compos Const 1998;2(4):175–85.
- [166] Teng JG, Lam L. Compressive behavior of carbon fiber reinforced polymer-confined concrete in elliptical columns. ASCE J Struct Eng 2002;128(12):1535–43.
- [167] Ye L, Yue Q, Zhao S, Li Q. Shear strength of reinforced concrete columns strengthened with carbon-fiber-reinforced plastic sheet. ASCE J Struct Eng 2002;128(12):1527–34.
- [168] Purba BK, Mufti AA. Investigation of the behavior of circular concrete columns reinforced with carbon fiber reinforced polymer (CFRP) jackets. Can J Civil Eng 1999;26:590–6.
- [169] Spoelstra MR, Monti G. FRP-confined concrete model. ASCE J Compos Const 1999;3(3):143–50.
- [170] Wang YC, Restrepo JI. Investigation of concentrically loaded reinforced concrete columns confined with glass fiber-reinforced polymer jackets. ACI Struct J 2001;98(3):377–85.
- [171] Tan KH. Strength enhancement of rectangular reinforced concrete columns using fiber-reinforced polymer. ASCE J Compos Const 2002;6(3):175–83.
- [172] Samaan M, Mirmiran A, Shahawy M. Model of concrete confined by fiber composites. ASCE J Struct Eng 1998;124(9):1025–31.
- [173] Toutanji HA. Stress-strain characteristics of concrete columns externally confined with advanced fiber composite sheets. ACI Mater J 1999;96(3):397–404.
- [174] Binici B. An analytical model for stress-strain behavior of confined concrete. Eng Struct 2005;27:1040–51.
- [175] Moran DA, Pantelides CP. Damage-based stress-strain model for fiber-reinforced polymer-confined concrete. ACI Struct J 2005;102(1):54–61.
- [176] Bisby LA, Dent AJS, Green MF. Comparison of confinement models for fiber-reinforced polymer-wrapped concrete. ACI Struct J 2005;102(1):62–72.
- [177] Saadatmanesh H, Ehsani MR, Li MW. Strength and ductility of concrete columns externally reinforced with fiber composite straps. ACI Struct J 1994;91(4):434–47.
- [178] Mirmiran A, Shahawy M. Behavior of concrete columns confined by fiber composites. ASCE J Struct Eng 1997;123(5):583–90.
- [179] Theriault M, Neale KW. Design equations for axially loaded reinforced concrete columns strengthened with fibre reinforced polymers wraps. Can J Civil Eng 2000;27:1011–20.
- [180] Chaallal O, Hassan M, Shahawy M. Confinement model for axially loaded short rectangular columns strengthened with fiber-reinforced polymer wrapping. ACI Struct J 2003;100(2):215–21.

- [181] Lam L, Teng JG. Design-oriented stress-strain model for FRP confined concrete. Constr Build Mater 2003;17:471–89.
- [182] Bisby LA, Green MF, Kodur VKR. Modeling the behavior of fiber reinforced polymer-confined concrete columns exposed to fire. ASCE J Compos Const 2005;9(1):15–24.
- [183] Saadatmanesh H, Ehsani MR, Jin L. Repair of earthquake-damaged RC columns with FRP wraps. ACI Struct J 1997;94(2):206–15.
- [184] Sheikh SA, Yau G. Seismic behavior of concrete columns confined with steel and fiber reinforced polymers. ACI Struct J 2002;99(1):72–80.
- [185] Harajli MH, Rteil AA. Effect of confinement using fiber-reinforced polymer or fiber-reinforced concrete on seismic performance of gravity load-designed columns. ACI Struct J 2004;101(1):47–56.
- [186] Ye LP, Zhang K, Zhao SH, Feng P. Experimental study on seismic strengthening of RC columns with wrapped CFRP sheets. Constr Build Mater 2003;17:499–506.
- [187] Xiao Y, Ma R. Seismic retrofit of RC circular columns using prefabricated composite jacketing. ASCE J Struct Eng 1997;123(10):1357–64.
- [188] Parvin A, Wang W. Concrete columns confined by fiber composite wraps under combined axial and cyclic lateral loads. Compos Struct 2002;58:539–49.
- [189] Elsanadedy HM, Haroun MA. Seismic design criteria for circular lap-spliced reinforced concrete bridge columns retrofitted with fiberreinforced polymer jackets. ACI Struct J 2005;102(3):354–62.
- [190] Karbhari VM, Eckel DA. Effect of cold regions climate on composite jacketed concrete columns. ASCE J Cold Reg Eng 1994;8(3):73–86.
- [191] Toutanji HA. Durability characteristics of concrete columns confined with advanced composite materials. Compos Struct 1999;44:155–61.
- [192] Kshirsagar S, Lopez-Anido RA, Gupta RK. Environmental aging of fiber-reinforced polymer-wrapped concrete cylinders. ACI Mater J 2000;97(6):703–12.
- [193] Karbhari VM, Rivera J, Dutta PK. Effect of short-term freeze-thaw cycling on composite confined concrete. ASCE J Compos Const 2000;4(4):191–7.
- [194] Karbhari VM. Response of fiber reinforced polymer confined concrete exposed to freeze and freeze-thaw regimes. ASCE J Compos Const 2002;6(1):35–40.
- [195] Naguib W, Mirmiran A. Flexural creep tests and modeling of concrete-filled fiber reinforced polymer tubes. ASCE J Compos Const 2002;6(4):272–9.
- [196] Toutanji H, Balaguru P. Durability characteristics of concrete columns wrapped with FRP tow sheets. ASCE J Mater Civil Eng 1998;10(1):52–7.
- [197] Toutanji HA, Balaguru P. Effects of freeze-thaw exposure on performance of concrete columns strengthened with advanced composites. ACI Mater J 1999;96(5):605–10.
- [198] Lee C, Bonacci JF, Thomas MDA, Maalej M, Khajehpour S, Hearn N, et al. Accelerated corrosion and repair of reinforced concrete columns using carbon fibre reinforced polymer sheets. Can J Civil Eng 2000;27:941–8.
- [199] Pantazopoulou SJ, Bonacci JF, Sheikh S, Thomas MDA, Hearn N. Repair of corrosion-damaged columns with FRP wraps. ASCE J Compos Const 2001;5(1):3–11.
- [200] Debaiky AS, Green MF, Hope BB. Carbon fiber-reinforced polymer wraps for corrosion control and rehabilitation of reinforced concrete columns. ACI Mater J 2002;99(2):129–37.
- [201] Scott RH. Intrinsic mechanisms in reinforced concrete beam-column connection behavior. ACI Struct J 1996;93(3):336–46.
- [202] Ghobarah A, Aziz TS, Biddah A. Rehabilitation of reinforced concrete frame connection using corrugated steel jacketing. ACI Struct J 1997;4(3):283–94.
- [203] Granata PJ, Parvin A. An experimental study on Kevlar strengthening of beam-column connections. Compos Struct 2001;53:163–71.
- [204] El-Amoury T, Ghobarah A. Seismic rehabilitation of beam-column joint using GFRP sheets. Eng Struct 2002;24:1397–407.

- [205] Antonopoulos CP, Triantafillou TC. Experimental investigation of FRP-strengthened RC beam-column joints. ASCE J Compos Const 2003;7(1):39–49.
- [206] Mirmiran A, Shahawy M, Samaan M. Strength and ductility of hybrid FRP-concrete beam-columns. ASCE J Struct Eng 1999;125(10):1085–93.
- [207] Li J, Bakoss SL, Samali B, Ye L. Reinforcement of concrete beamcolumn connections with hybrid FRP sheet. Compos Struct 1999;47:805–12.
- [208] Ghobarah A, Said A. Shear strengthening of beam-column joints. Eng struct 2002;24:881–8.
- [209] Gergely J, Pantelides CP, Reaveley LD. Shear strengthening of RCT-joints using CFRP composites. ASCE J Compos Const 2000;4(2):56–64.
- [210] Corry RW, Dolan CW. Strengthening and repair of a column bracket using a carbon fiber reinforced polymer (CFRP) fabric. PCI J 2001:54–61.
- [211] Pulido C, Saiidi MS, Sanders D, Itani A, El-Azazy S. Seismic performance of two-column bents – part I: retrofit with carbon fiber-reinforced polymer fabrics. ACI Struct J 2005;101(4): 558–68.
- [212] Shannag MJ, Alhassan MA. Seismic upgrade of interior beamcolumn subassemblages with high-performance fiber-reinforced concrete jackets. ACI Struct J 2005;102(1):131–8.
- [213] Ahmad SH, Zia P, Yu TJ, Xie Y. Punching shear tests of slabs reinforced with 3D carbon fiber fabric. ACI Con Int Des Const 1994;16(6):36–41.
- [214] Banthia N, Al-Asaly M, Ma S. Behavior of concrete slabs reinforced with fibre-reinforced plastic grid. ASCE J Mater Civil Eng 1995;7(4):252–7.
- [215] Shahawy MA, Beitelman T, Arockiasamy M, Sowrirajan R. Experimental investigation on structural repair and strengthening of damaged prestressed concrete slabs utilizing externally bonded carbon laminates. Compos: Part B 1996;27:217–24.
- [216] Garden HN, Hollaway LC, Thorne AM. A preliminary evaluation of carbon fibre reinforced polymer plates for strengthening rein-

forced concrete members. Proc Inst Civil Eng Struct Build 1997;123:127-42.

- [217] Kumar SV, GangaRao HVS. Fatigue response of concrete decks reinforced with FRP rebars. ASCE J Struct Eng 1998;124(1):11–6.
- [218] Michaluk CR, Rizkalla SH, Tadros G, Benmokrane B. Flexural behavior of one-way concrete slabs reinforced by fiber reinforced plastic reinforcements. ACI Struct J 1998;95(3):353–65.
- [219] Matthys S, Taerwe L. Concrete slabs reinforced with FRP grids I: one-way bonding. ASCE J Compos Const 2000;4(3):145–53.
- [220] Matthys S, Taerwe L. Concrete slabs reinforced with FRP grids II: punching resistance. ASCE J Compos Const 2000;4(3):154–61.
- [221] Lam L, Teng JG. Strength of RC cantilever slabs bonded with GFRP strips. ASCE J Compos Const 2001;5(4):221–7.
- [222] Yost JR, Goodspeed CH, Schmeckpeper ER. Flexural performance of concrete beams reinforced with FRP grids. ASCE J Compos Const 2001;5(1):18–25.
- [223] Seim W, Horman M, Karbhari V, Seible F. External FRP post strengthening of scaled concrete slabs. ASCE J Compos Const 2001;5(2):67–75.
- [224] Binici B, Bayrak O. Use of fiber-reinforced polymers in slab-column connection upgrade. ACI Struct J 2005;102(1):93–102.
- [225] Chen CC, Li CY. Punching shear strength of reinforced concrete slabs strengthened with glass fiber-reinforced polymer laminates. ACI Struct J 2005;102(4):535–42.
- [226] El-Sayed A, El-Salakawy E, Benmokrane B. Shear strength of oneway concrete slabs reinforced with fiber-reinforced polymer composite bars. ASCE J Compos Const 2005;9(2):147–57.
- [227] Limam O, Nguyen VT, Foret G. Numerical and experimental analysis of two-way slabs strengthened with CFRP strips. Eng Struct 2005;27:841–5.
- [228] Oh H, Sim J, Meyer C. Fatigue life of damaged bridge deck panels strengthened with carbon fiber sheets. ACI Struct J 2005;102(1):85–92.
- [229] Stark A, Binici B, Bayrak O. Seismic upgrade of reinforced concrete slab-column connection using carbon fiber-reinforced polymers. ACI Struct J 2005;102(2):324–33.